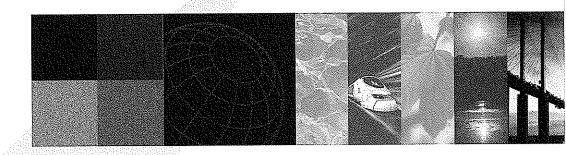
# **Halcrow Maritime**

Poole and Christchurch Bays
Shoreline Management Plan
Volume 3 - Developed and Natural Environment
March 1999



Halcrow

# **Halcrow Maritime**

Poole and Christchurch Bays
Shoreline Management Plan
Volume 3 - Developed and Natural Environment
March 1999

Halcrow Maritime
Burderop Park Swindon Wiltshire SN4 0QD
Tel +44 (0)1793 812479 Fax +44 (0)1793 812089
www.halcrow.com

Halcrow Maritime has prepared this report in accordance with the instructions of their client for their sole and specific use. Any other persons who use any information contained herein do so at their own risk.

### **PREFACE**

This is the Consultation Draft of the Poole and Christchurch Bays Shoreline Management Plan. It sets out the strategy for management of coastal defences between Durlston Head in Dorset and Hurst Spit in Hampshire, including Poole and Christchurch Harbours (Subcell 5F). The SMP has been prepared by Halcrow Maritime on behalf of the Poole and Christchurch Bays Coastal Group.

The SMP is divided into the following 4 volumes:

### **VOLUME 1 – STRATEGY DOCUMENT**

### PART A: INTRODUCTION

Sets out the background to, and role of, the SMP, along with its aims and objectives.

# PART B: HOW TO USE THE PLAN

Describes the key elements of strategy presentation, in the Process and Management Unit sections.

# PART C: PROCESS UNIT DESCRIPTIONS

Present a synopsis of the main characteristics of each Process Unit, summarised from Volumes 2 and 3.

### PART D: MANAGEMENT UNIT STATEMENTS

Divided into two sections, Part D1 presents the 'Management Unit Characteristics' and Part D2 the 'Appraisal of Strategic Options' which identifies the preferred option along with implementation and monitoring guidance.

### PART E: FUTURE DEVELOPMENT

Describes where/how current understanding needs to be improved and gives a suggested time frame for both the review of the strategies and, further into the future, for a more comprehensive reappraisal of the Plan as a whole.

### **VOLUME 2 - PHYSICAL ENVIRONMENT**

### PART A: GEOLOGY AND GEOMORPHOLOGY

Presents the physical characteristics of the shoreline along with its the formative geomorphological history, and describes the subdivision of the coast into Process Units.

# PART B: COASTAL CONDITIONS

Describes the wind, wave, tide and current regimes driving contemporary coastal processes.

# PART C: SHORELINE EVOLUTION

Identifies and reviews historical evolution of the shoreline, both 'natural' and due to Mans intervention.

### PART D: CONCEPTUAL SEDIMENT PROCESS MODELS

Provides qualitative and quantitative information about sediment processes within Poole and Christchurch Bays, in addition to setting longer term assessments of how the coast is likely to be impacted upon.

# ANNEX A: ISSUES ANALYSIS AND STATEMENT OF OBJECTIVES

Presents shoreline management issues and associated objectives, relevant to the Physical Environment of the coast, identified during public consultation on the SMP.

# **VOLUME 3 – DEVELOPED AND NATURAL ENVIRONMENT**

# PART A: COASTAL DEFENCES

Examines the current state of knowledge of coastal defences, and where possible reviews the nature and standard of defence provided, and their suitability to provide the standards required in the future.

# PART B: DEVELOPED ENVIRONMENT

Human use of the shoreline is assessed through descriptions of land use, coastal activities, offshore use and archaeological interest, and requirements for coastal defence planning.

### PART C: NATURAL ENVIRONMENT

Reviews landscape, habitat and earth science conservation value of the shoreline, and the key issues relating to coastal defence provision.

# PART D: PLANNING

Detail present planning procedures and sets out existing policies and objectives, of both statutory and non-statutory plans, of relevance to coastal defence.

# PART E: LIST OF RELEVANT DOCUMENTS

A bibliographical listing of those documents/sources used during the production of the SMP.

# ANNEX A: ISSUES ANALYSIS AND STATEMENT OF OBJECTIVES

Presents shoreline management issues and associated objectives, relevant to the Developed and Natural Environment of the coast, identified during public consultation on the SMP.

# **VOLUME 4 – MAPS AND SUPPORTING INFORMATION**

Maps presented in Parts A to D are at 1:25,000 scale.

# PART A: DEVELOPED ENVIRONMENT MAPS

These base maps illustrate the land use of the area, categorised into ten classifications.

### PART B: CONSERVATION MAPS

Includes details of all international, national and local conservation designations, whether statutory or non-statutory. Archaeological and historical features of a terrestrial and maritime nature are also depicted.

# PART C: COASTAL DEFENCES

The extent and nature of all forms of coastal defence have been mapped.

# PART D: PHOTOGRAPHS

A series of photographs representative of each Process Unit.

A consistent page numbering style has been used throughout Volumes 1 to 3, as follows:

Volume – Part Page.

For example, 1-A4 is Volume 1 Part A Page 4.

# INTRODUCTION TO THIS VOLUME

During their development of SMPs around the country, Halcrow have been able to witness, at first hand, the "evolution" of the SMP process and have subsequently been involved in many useful discussions and exchanges of ideas. One important outcome of this has been the proposal of adopting wider remit "Process Units" which Halcrow advocated and used in 1996 (Suffolk Shoreline Management Plan).

The structure of this Volume has been set out in the same vein, purposely to assist in the preparation of the Volume 1 Strategy Document. Therefore, the following text has been produced to clarify why and how the study area has been divided up the way it has and also to provide an indication of how this breakdown will be used effectively during Phase 2.

### WHY SET UP PROCESS UNITS?

The key to achieving effective and sustainable management of the shoreline is linked to a sound knowledge of coastal processes and their interaction along the coast. All management decisions ought therefore to be linked primarily to the processes and their implications. Management strategies need to address these implications on a broader scale than land use alone and the defence options for individual management units must be appraised against the overall processes within a larger area. The structure of the management for Poole and Christchurch Bays is therefore one where conformity with the requirements of the Process Unit is paramount. Therefore, it is for these reasons that the Process Unit framework has been set up for this SMP.

The basic building block for the development of policies within an SMP is the "Management Unit". In the MAFF Guidelines (1993), a management unit is defined as "a length of shoreline with coherent characteristics in terms of both natural coastal processes and land use". The Guide goes on to say that "these are likely to constitute discreet benefit areas at the economic appraisal stage". For this SMP, a broader more strategic approach is to be adopted that takes into consideration wider issues and impacts that should, over the long term, provide a more useful framework from which to manage the shoreline.

The groundwork for using this approach has been set within this Volume and, where possible, the final strategy Document (Volume 1) of the SMP will utilise this to its fullest effect.

### **HOW ARE PROCESS UNITS IDENTIFIED?**

The sub-cell system derived from the "Mapping of Littoral Cells" report commissioned by MAFF in 1993 (Motyka and Brampton) originally categorised sub-cells on the direction and movement (littoral drift) of sand and gravel along beaches. Two main types of boundary between cells were recognised, firstly at littoral drift divides and secondly at sediment sinks (Motyka and Brampton, 1993). It was stressed in this report that the division into coastal cells is strictly applicable to the purpose of coastal defence management on non-cohesive beaches (such as Poole and Christchurch Bays). The direction and movement of sediment further offshore is unlikely to mirror littoral drift directions and boundary conditions in all cells.

Based upon the Terms of Reference set out for this SMP, the shoreline of the subcells shall be divided into discrete "Process" and associated "Management Units". A Process Unit is defined in the Consultants Brief as being "a length of shoreline with coherent characteristics in terms of processes and based upon an understanding of the geology and geomorphology, the prevailing sea conditions

and natural shoreline evolution". This is seen as a necessary development of the present MAFF Guidelines and one that is required to ensure sustainable management techniques are followed on the coast.

An important clarification to make is that the demarcation of these Process Units is not merely made on the geographic limits of certain physical features or landforms. Different coastal characteristics (such as dune, storm ridge or marsh) should <u>not</u> be separately divided based purely on the fact that they are very different in their morphological appearance. On the contrary, their formation is likely to be attributed to linked coastal processes that have occurred over a range of temporal scales. In addition to this, their integrity is dependent upon sedimentary budget regimes that act over a far wider scale than the geographic limits of a certain coastal feature.

With reference to Poole and Christchurch Bays, there is a strong physical relationship between areas of open coast and sediment sink areas (such as Poole and Christchurch Harbours). Consequently, interlinkages will and do occur especially between areas, such as harbour mouths and the open coast. There are also key strategic landforms (terrestrial or subtidal, such as Hook Sand or Double Dykes) where actions in one Process Unit may well be influential on the natural evolution of another. Therefore, the concept of introducing Process Units that emphasise links with adjacent units is ultimately required. This shall be assisted through the use of Process Unit Statements. The wordings used for these shall be presented in more detail during the development of Volume 1 ("The Strategy Document") and shall be subject to review and general acceptance from the Coastal Group.

# **HOW ARE PROCESS UNITS DEFINED?**

The following definition has been created to explain a Process Unit. It is described as:

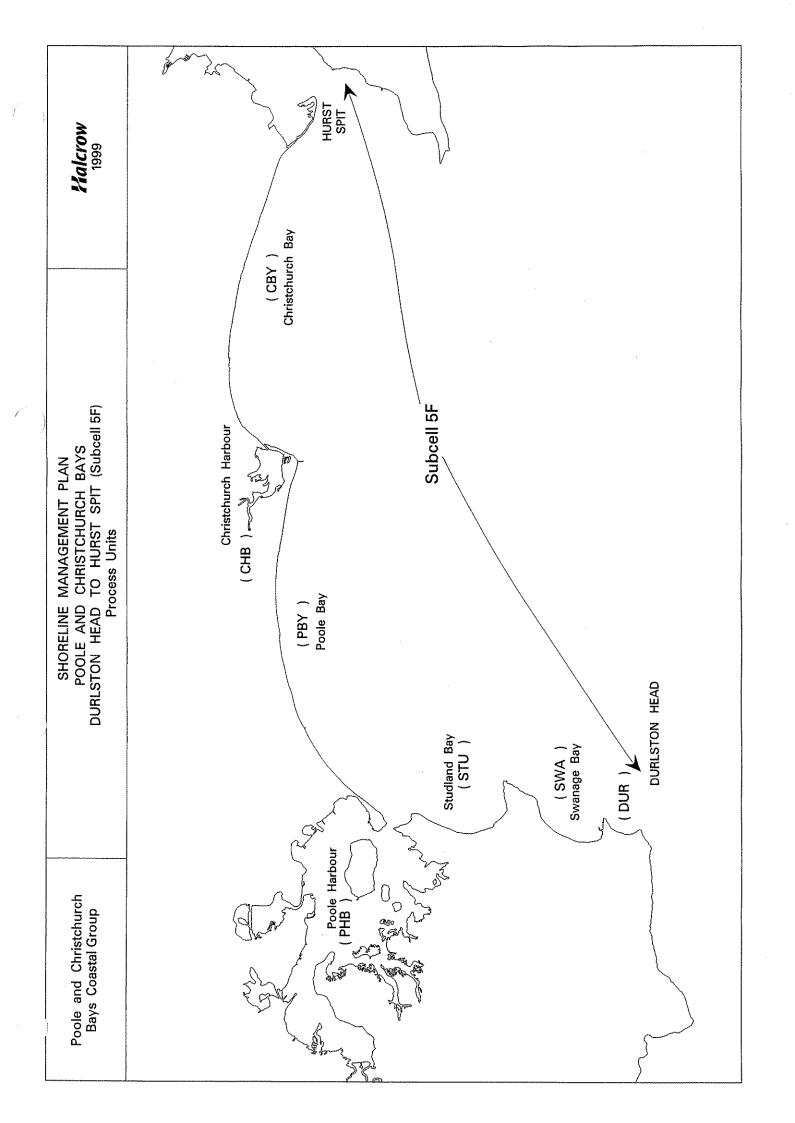
"an area of coastline reflecting the complexity or simplicity of a particular coastal area, not merely representing lengths of coherent physical characteristics, but considering aspects of related littoral interdependencies that impact upon both ecological and geomorphological evolutionary trends over a range of spatial and temporal scales"

### WHERE ARE THESE PROCESS UNITS?

There are seven Process Units established for this SMP, based primarily on the identification of landforms, critical coastal processes (waves, currents), their interlinkages and variability giving special attention to their position and function within the overall sub-cell.

The Process Units, from east to west around the sub-cell (see opposite), are as follows:

5F-1	Hurst Spit to Hengistbury Head Long Groyne
5F-2	Christchurch Harbour
5F-3	Hengistbury Head Long Groyne to Sandbanks Ferry Slipway
5F-4	Poole Harbour
5F-5	South Haven Point to Handfast Point
5F-6	Handfast Point to Peveril Point
5F-7	Peveril Point to Durlston Head



# **HOW THE PROCESS UNIT FRAMEWORK INTENDS TO OPERATE?**

The Process Unit framework, in very simple terms, has enabled the various topic areas to be conveniently divided up into manageable areas. This has been followed for the contents of Volumes 2 and 3 of the SMP as shown below:

### Volume 2

- · Geology / Geomorphology
- Coastal Conditions
- Shoreline Evolution
- Conceptual Sediment Process Models

### Volume 3

- Coastal Defences
- Developed Environment
- Natural Environment
- Planning

In addition to this and from a more strategic view, the two tier "Process" and "Management Unit" approach will also prove most useful on two accounts. Firstly, it shall enable long term options (ie: long term sustainability) to be developed that will permit free operation of key process components (ie:geomorphological evolution). Secondly, shorter term measures may be set out for individual shorter management units so long as management decisions comply to the longer term objective of an area and thus are not detrimental to processes over a broader timescale.

### WHAT COMES NEXT?

The results of the Phase 1 studies (Volumes 2,3 and 4) represent a detailed understanding of the processes and issues relating to Poole and Christchurch Bays. At this point, the division into Process Units and Management Units can be confirmed and the detailed objectives for each Unit established. These will be forwarded under separate cover to a draft level.

The next step (Phase 2) will be to determine the appropriate policy for each of these Units taking into account the various pressures and conflicts of interests that exist, and establish the preferred strategic coastal defence options to achieve these policy requirements. This needs to take into account all of the issues and objectives identified. Additional information to be established will be the standards of service required by any future defence policy and the economic justification for providing protection. The MAFF guide to coastal defence authorities on Shoreline Management Plans describes four generic strategic options for defence. The SMP will adopt these as a baseline but not be restricted by them, ie: elaboration on these options will be put forward particularly in terms of time frame strategies (long and short term actions).

Presentation of the strategies will be in the form of individual Management Unit Statements which summarise the main information and issues, and show the rationale behind the strategic decisions that have been proposed. Recommendations will also be made on how the strategic coastal defence options should be implemented, to justify their suitability as a sustainable solution. The Statements will include descriptive maps indicating the key aspects for each unit.

# Part A

# **COASTAL DEFENCES**

Volume 1 of the SMP shall identify future strategic coastal defence options. As a precursor to this, there is a need to consider how the shores of Poole and Christchurch Bays have been defended in the past and what exists today. The nature of these defences may be influential upon the evolution of the coast, whilst their condition can provide guidance on the sustainability of particular options. It is also necessary to know the adequacy of these defences to provide the standards of service required to protect the assets that lie behind them.

This section determines the current state of knowledge and existence of information relating to defences around the coast. Where adequate information exists, this has been used for assessing the standards of defence provided at present and thus the suitability of such defences to provide the standards required for the future.

# **COASTAL DEFENCES**

# **CONTENTS**

1	INTRODUCTION						
	1.1	Format of	this Report	1			
2	COAS	STAL DEFEN	CE ADMINISTRATION	2			
3	REVI	REVIEW OF INFORMATION SOURCES / USEFUL REFERENCES					
	3.1	Introduction	on	3			
	3.2	Coast Pro	tection Survey of England	3			
	3.3	Sea Defence Survey					
	3.4	Other Sources					
4	ASSE	ASSESSMENT OF COASTAL DEFENCE SITUATION					
	4.1	General					
	4.2	Information Provided					
	4.3	Methods o	f Assessment	5			
		4.3.1	General	5			
		4.3.2	Outline Approach	5			
		4.3.3	Methods Applied	6			
	4.4	Survey Re	sults	8			
5	REVIE	W OF COAS	STAL DEFENCES	9			
	5.1	Hurst Spit	to Hengistbury Head Long Groyne – (5F-1)	9			
		5.1.1	Description of Defences	9			
		5.1.2	Assessment of Defence Standard	14			
	5.2	Christchur	ch Harbour – (5F-2)	15			
		5.2.1	Description of Defences	15			
		5.2.2	Assessment of Defence Standard	16			
	5.3	Hengistbury Head Long Groyne to Sandbanks Ferry Slipway – (5F-					
		5.3.1	Description of Defences	<b>17</b> 17			
		5.3.2	Assessment of Defence Standard	20			
	5.4	Poole Hark	oour - (5F-4)	21			
		5.4.1	Description of Defences	21			
		5.4.2	Assessment of Defence Standard	25			
	5.5						
		5.5.1	Description of Defences	<b>25</b> 25			
		5,5.2	Assessment of Defence Standard	26			
	5.6						
		5.6.1	Description of Defences	26			
		5.6.2	Assessment of Defence Standard	28			
	5.7	Peveril Poi	int to Durlston Head – (5F-7)	28			
		5.7.1	Assessment of Defences	28			
		5.7.2	Assessment of Defence Standard	28			
	5.8	Assessme	nt of Condition of Foreshore on Defence Structure	28			
		581	Hurst Spit to Hengisthury Head Long Grovne (5E-1)	20			

# Poole and Christchurch Bay's Shoreline Management Plan: Stage Two

5.8.2	Christchurch Harbour – (5F-2)	29
5.8.3	Hengistbury Head Long Groyne to Sandbanks Fery	Slipway
	- (5F-3)	29
5.8.4	Poole Harbour – (5F-4)	29
5.8.5	South Haven Point to Handfast Point – (5F-5)	30
5.8.6	Handfast Point to Peveril Point - (5F-6)	30
5.8.7	Peveril Point to Durlston Head - (5F-7)	30

# **GLOSSARY OF TERMS**

# REFERENCES

# **TABLES**

# **APPENDICES**

Appendix A Survey Report Tables
Appendix B Sands Beach Cross Sections

### 1 INTRODUCTION

# 1.1 Format of this Report

This report on coastal defences is divided into 5 sections. Following this introduction, Section 2 describes the general situation with regard to coastal defence administration. Proposed procedures for future co-operation between authorities and other bodies for the undertaking of work are contained within other sections of the report. In Section 3, an overview of existing information sources and the quality/usefulness of details contained therein is provided. Section 4 explains the approaches / methods that have been adopted in developing this Shoreline Management Plan to assess the existing coastal defence situation, whilst Section 5 provides details on the defences themselves.

Section 5 is structured according to the delineation of coastal process units. For each, information is provided on where defences already exist and their general nature, the ownership of defences, and the authorities who have local defence responsibilities or powers.

### 2 COASTAL DEFENCE ADMINISTRATION

The administration of coastal defences falls into two distinct areas: coast protection, the protection of land from erosion or encroachment by the sea, and sea defence (or flood defence) which is the protection of land from inundation by the sea.

The Coast Protection Act 1949 provides maritime district councils with permissive powers to carry out coast protection works. They are also responsible for regulating any works carried out by others (the primary responsibility for protecting land or property lies with the owner).

Both the Maritime District Councils and the Environment Agency have powers to carry out defence works. Under the Water Resources Act 1991, the Environment Agency has a duty to exercise a general supervision for flood defences, which may be their own defences or regulating the defence works of others. Any proposals affecting such defences must have the consent of the Environment Agency. The powers to carry out new works are again, however, permissive. Local authorities also have powers to carry out flood defence works.

Coast protection works and flood protection are promoted by the operating authorities where there is benefit to the community. MAFF are responsible for making available grants towards capital expenditure under both Acts, subject to these being environmentally acceptable, technically sound and economically worthwhile.

Coastal defence has previously been established as relating to areas on the coast and within creeks or estuaries up to certain points. The areas where the term coastal defence no longer applies have previously been determined and are referred to as the Schedule 4 boundaries, as defined by the 1949 Coast Protection Act (including subsequent amendments), which for this region are:

The River Frome, at Turner's Cove

The River Piddle, at Buck's Cove

The River Sherford,

The River Stour and Avon, at Clay Pool

Some of these boundaries have been somewhat arbitrarily determined and bear little relationship to coastal processes. Nevertheless, the existing coastal defences are identified as those which lie seaward of these agreed limits. However, this is an issue as it has implications for the amount of grant aid made available.

### 3 REVIEW OF INFORMATION SOURCES / USEFUL REFERENCES

### 3.1 Introduction

Most information regarding existing defence along this coastline is available from either the local authorities, the Environment Agency or MAFF. The two sources of greatest importance are the Coast Protection Survey of England (CPSE) and the Sea Defence Survey (SDS). These both provide essential information for the Shoreline Management Plan.

# 3.2 Coast Protection Survey of England

The CPSE (1994) was commissioned by MAFF and details all defences which have been constructed to protect against coastal erosion. These defences are often the responsibility of the individual local authority, although a number are maintained by others such as the County Council, harbour authorities and various private owners.

Volumes 5 and 6 of the CPSE contain the details for this region and comprise maps, photographs, outline cross sections and tabulated defence details. The latter includes details on location, structure type and material, condition, residual life and ownership. This is also available in digital database format. The CPSE digital database is updated annually to incorporate more recent changes and/or errors in the original data.

Defence information is divided by defence lengths and defence elements. Changes in defence length occur where there is a significant change in the construction, ie a change in the form of the structure, whilst defence elements are defined as the individual components of the structure. This provides a relatively clear identification of the individual defences and, combined with the sections, photographs and maps, gives very good quality information. Maps illustrating the geographical extent of the defences described are reproduced in Figures 3.1 to 3.8 (see Volume 4).

# 3.3 Sea Defence Survey

The remaining defences along this coastline is included in the SDS (1990/91), which was commissioned by the NRA (now incorporated into the Environment Agency). This details all of the defences which provide flood defence. Whilst the Environment Agency has a general supervisory duty for such flood defence, the majority of the defences within the region covered by this Shoreline Management Plan are owned or maintained by others such as the local authorities or private owners.

This information was recorded in three phases. Phase I contained details of the then NRA-owned defences, whilst phases 2 and 3 comprised those flood defences maintained by the local authorities and private owners. Details are provided in a series of reports with separate volumes for Phase 1 and one volume for each of the local authority districts. These contain cross sections of each defence and tabulated details including location, structure type and material, condition, residual life and ownership. Again, these details are also available in digital database format. Phase 4 of the survey details tidal defences in all ownershps.

Like the CPSE, defence information is divided between defence lengths and defence elements. However, distinction between different structures is more

difficult with elements sometimes denoting a sectional change and for other defences indicating a longitudinal change.

It should be noted that at some locations there is considerable overlap between the CPSE and the SDS. Phases 1-3 of the SDS is reviewed annually by the Environment Agency. The defence numbering system is currently being revised to recognise process and management units.

### 3.4 Other Sources

In 1989, HR Wallingford produced 'A Macro Review of the Coastline of England and Wales' for MAFF. This describes the coastline for the whole region and complements the CPSE and SDS information. The details provided on man-made defences are not extensive. However, information on the natural condition of the coast is combined to give a useful overview and appreciation of the setting for these defences. There are other documents which provide an overview of the coastal defence situation in the region, such as the JNCC reports in their series 'Coasts and Seas of the United Kingdom'. These provide broad information but are generally not sufficiently detailed to provide additional information for the Shoreline Management Plan.

A number of documents provide legislation, policy and guidance on strategic defence. Where relevant these are referred to elsewhere within this Shoreline Management Plan (see report on Planning Issues). The 1993 MAFF publication 'Project Appraisal Guidance Notes' provides indicative standards of protection that should be sought for different situations. Of particular relevance is 'Coastal Defence and the Environment - A guide to good practice' (1993) produced by MAFF which discusses particular techniques and approaches for a range of defence situations. Another document with similar details is the 'Guide to the Selection of Appropriate Coast Protection Works for Geological SSSIs' (1991), by HR Wallingford.

There are a number of other guides which are of use in assessing the standard of service offered by defences and these should be consulted when doing so. The best current practice is well defined by the CIRIA/CUR publication 'Manual on the Use of Rock in Coastal and Shoreline Engineering' (1991) and the CIRIA 'Beach Management Manual' (1996) with their attendant references.

Each of the local authorities and the Environment Agency hold various details of some of their own structures, particularly those built or refurbished during the past 20 years. Much of the detailed information relates to construction, ie drawings, and specifications. There are also a number of structure inspection reports which provide information on the condition of some of the older defences, giving details of their composition. In addition there are Engineers Reports for some schemes, which are also held by MAFF. However, whilst these vary in their extent of information, in general these do not contain much information of further use.

Some of these scheme and construction details will be of use in subsequent stages when it comes to the future implementation of the Shoreline Management Plans, but they are not required for development of the strategy options.

### 4 ASSESSMENT OF COASTAL DEFENCE SITUATION

### 4.1 General

The existing defence situation within each individual stretch of coastline has been assessed and is detailed in Section 5. This is initially based upon the data available from the CPSE, the SDS, and discussions with members of the Coastal Group. This provided good background on the existing situation regarding the defences and any existing coastal erosion and flooding issues. This has been supplemented by the provision of any additional defence details from the authorities.

# 4.2 Information Provided

Section 5 is structured by coastal process unit for convenience of presenting the information. For each process unit, details are given on which authorities/organisations have defence responsibilities or powers.

Within each process unit, further sub-division is made by location for ease of reference. At each location details are provided on the defences, type, length, ownership (although this should not necessarily be regarded as also suggesting a right of responsibility) and any existing reference/codes relating to present record systems. To provide a consistent overview of all of the defences within each area, data from the most recent update of the CPSE and Phases 1, 2 and 3 of the SDS have been combined.

### 4.3 Methods of Assessment

### 4.3.1 General

The Study has assessed the effectiveness of the existing defences. The objective of this exercise is to identify any unsatisfactory links in the line of defence in the study area. This objective has been satisfied by identifying the standard of service provided by the existing defence, whilst at the same time considering the envisaged longevity of the defence inferred by assessments of their condition and residual life.

In their Project Appraisal Guidance Notes (PAGN) (MAFF, 1993), the Ministry of Agriculture, Fisheries and Food (MAFF) define the standard of service as '... the annual probability that a sea wall, flood bank etc will encounter conditions even more severe than those for which it was designed.' In the absence of such design information, overtopping discharge threshold limits (recommended for design where wave overtopping is to be allowed) have been adopted. Indicative standards of protection are set out in PAGN Annex K, with varying levels according to the land use at risk.

The results of the assessment are presented in Tables 4.1 to 4.14 and illustrated graphically on Figs 3.1 to 3.8 (see Volume 4).

# 4.3.2 Outline Approach

The appraisal comprises four components:

- (a) overflow
- (b) overtopping
- (c) residual life
- (d) undermining

The standard of service achieved by a typical section under overflow and overtopping conditions is identified. The results are then combined to give an overall standard.

Residual life for the most part matches the CPSE/SDS assessment.

By identifying low lying foreshores that are undergoing erosion, and observing if they occur at locations where the defence structure depends on a high foreshore level, it has also been possible to make preliminary assessments of the likelihood of these structures experiencing some kind of toe failure in the future.

The wave and water level conditions used for the analyses were those presented in Chapter 3 of this document.

All of the analyses were repeated to allow for sea level rise. This was assumed to be 6mm per year, the figure stipulated in PAGN, Annex H.

# 4.3.3 Methods Applied

### Overflow

Over flow occurs when the prevailing water level is greater than the crest height of the defence.

The overflow analysis consists of comparing the water levels, established by joint probability analysis for water levels and wave heights for different return periods, against the crest level of the defence. When the crest is exceeded, the defence has failed in overflow. The actual standard of service of the defence in terms of overflow is thus the highest return period for which the defence passed the overflow test.

# Overtopping

Each type of defence structure has a critical level of wave overtopping that it can withstand before structural damage occurs. This is dependant upon parameters such as whether the defence is an embankment type structure having a back slope which allows overtopping water to run down, or seawall type structures. The type of construction of both these defence types also has a significance as to the overtopping volumes it can withstand, eg grassed embankments being more susceptible to washout than revetted ones, soft cliffs above defences having greater likelihood of erosion than hard cliffs. The following are critical overtopping rates for various structure types, which have been determined from analysis of damage occurrence from actual events (Goda, 1971) and remain in use today as standard criteria (eg CUR/CIRIA, 1991):

Type of seawall construction	Threshold of critical overtopping litres/sec/m run
Seawall with backslope (Embankment)	
Crest and backslope unprotected	5
Crest protected and backslope unprotected	20
Crest and backslope protected	50
Seawall without backslope (Revetment)	
Apron unpaved	50
Apron paved	200

The type of defences along this coastline vary from simple beaches to concrete walls which are either vertical or sloping. To analyse these structures correctly it was necessary to use a number of different methods, each one being for a specific structure type. For sloping, simple and bermed, revetments, seawalls and embankments Owen's formulae are used to determine the wave overtopping volumes (HR Wallingford report EX924, "Design of Seawalls allowing for wave overtopping",1990). Where such structures incorporate a crest or wave return wall. the method outlined in the HR Wallingford report SR261 "Effectiveness of recurved wave return walls", Owen and Steel, 1991 was used. Vertical wall structures were analysed using the recently published method by Besley, Stewart and Allsop, (HR Wallingford), "Overtopping of vertical structures: new prediction methods to account for shallow water conditions", proceedings ICE International Conference on Coastlines, Structures and Breakwaters, 1998. Finally, where it has been necessary to analyse natural defences only, the method used was that presented by Van der Meer within "A code for dike height design and examination", also published within the proceedings ICE International Conference on Coastlines, Structures and Breakwaters, 1998.

Overtopping analysis has been performed for two different scenarios as follows:

- present day conditions;
- increase in storm exposure to allow for 50 years of sea level rise;

For each scenario, the overtopping rates associated with the joint occurrence of waves and water levels for return periods of between 1 and 100 years have been calculated. The results of the wave overtopping have been summarised in Tables 4.1 to 4.14. In each case the standard of service of the defence was taken as the highest return period for which it passed the overtopping test.

Assessment of present day conditions considered the existing situation, ie present predictions of waves and water levels, together with the beach profiles.

Allowance for sea level rise used the same information but considered an increase in water levels over 50 years, and the consequent increase in wave exposure that would also occur.

The wave and water level data (including sea level rise predictions) used for the analyses were those derived at representative locations around the coast and within the harbours as presented in the coastal processes section of the report. This established the nearshore conditions, however, wave characteristics will

further alter as they travel through the inshore zone and up the beach. Shallow water wave characteristics have therefore also been studied to determine actual extreme wave conditions for different return periods coincident with each water level of similar return period. Consideration has been given to changes in beach slope, using the survey profiles, adopting the methods of Goda (1985) and ENDEC (presented in CUR/CIRIA 1991).

### Residual Life

The CPSE and SDS both contain an assessment of the residual life of each of the defence elements which they describe. Both surveys have recently been reviewed and updated by local authorities and the Environment Agency. There being no scope for the detailed field appraisal of all structures, the surveys are considered to provide a sufficiently accurate appraisal of the life expectancy of each element.

The two surveys have different time bands of residual life into which the defences were placed. The CPSE has the following bands:

- > 10 years
- 5 10 years
- < 5 years

whilst the SDS employs the following classification system:

- > 5 years
- 2 5 years
- < 2 years

# Undermining

The methodology adopted for assessing the susceptibility of defences to undermining is described in Section 6.8.

# 4.4 Survey Results

Selected extracts from the updated versions of the CPSE and SDS databases are reproduced in Appendix A at the end of this Chapter. Maps illustrating the geographical extent of the defences described are reproduced on Figures 3.1 to 3.8 (see Volume 4). A separate glossary of terms used in the description of the Defence Lengths and Defence Elements is also provided.

### 5 REVIEW OF COASTAL DEFENCES

The following sections contain the review of coastal defence details for each of the coastal process units as follows:

Area 5F-1 Hurst Spit to Hengistbury Head Long Groyne

Area 5F-2 Christchurch Harbour

Area 5F-3 Hengistbury Head Long Groyne to Sandbanks Ferry Slipway

Area 5F-4 Poole Harbour

Area 5F-5 South Haven Point to Handfast Point

Area 5F-6 Handfast Point to Peveril Point

Area 5F-7 Peveril Point to Durlston Head

For each process unit, the structures within that unit are described in terms of their location, form, nature, condition and ownership and their susceptibility to overflow. Selected typical defences within each unit are assessed to establish their effectiveness, sufficiency and the standard of service provided under extreme wave conditions. Appraisals of areas identified as being at risk from erosion as a result of a low level eroding foreshore and other influences are included.

Defence length numbers from the Coast Protection Survey and Sea Defence Survey are used eg 2757 (CPSE) and 071/1055D (SDS).

# 5.1 Hurst Spit to Hengistbury Head Long Groyne – (5F-1)

The existing defence structures in area 5F-1 are predominantly seawalls and rock armour revetments with timber groynes. The coastline consists of sandy beaches to the east and steeper shingle beaches to the west.

# 5.1.1 Description of Defences

Mudeford Quay is a low-lying former sandbank at the entrance to Christchurch Harbour which is now fronted by sheet piled walls and promenades. Further east, the promenade is fronted by a sand beach and rock groynes. The ground levels behind gradually rise from Friars Cliff where the sand beach widens towards Highcliffe.

From Highcliffe the beaches change to predominantly steep and shingle with lower sand foreshore. The cliffs gradually decrease in height, from 25 m at Naish Farm to below 8 m at Milford-on-Sea. Further east past Milford-on-Sea, the shingle beach continues and widens to form the embankment at Hurst Spit.

Hurst Spit shelters the Western Solent from the more aggressive wave climate in Christchurch Bay. The defences recently reconstructed in the Keyhaven and Pennington areas have been based on the assumption that Hurst Spit will continue to act as a barrier to waves entering the Western Solent. Indeed, the standard of protection afforded by all the defences in the Western Solent would have to be reviewed if Hurst Spit were to breach. Furthermore, there is clear evidence that the saltmarshes in the Lymington and Keyhaven areas will be adversely affected by any depletion of shingle levels on Hurst Spit ("Western Solent Saltmarsh Study", A Bradbury). Thus, Hurst Spit is of great significance to the coastal defences in this region.

Hurst Spit continues eastwards from Saltgrass Lane to its eastern tip over a length of 2.28 km. The shingle on Hurst Spit consists of eroded cliff material transported alongshore from Christchurch Bay. Coast protection measures throughout Christchurch Bay have reduced the supply of sediment. Indeed, the Spit has been

breached on several occasions in its recent history. The first recorded breach was in 1962 (HR Wallingford, EX 1601, 1987). There were further breaches in 1984 and in 1989. The damage due to the storms in December 1989 are described in the "Lymington/Pennington Flood Investigation", (NRA – Southern Region, 1990). Periodic nourishment has been undertaken to build up levels along Hurst Point, starting in 1981/1982. A £5 million coast protection scheme was carried out in 1996 to build up the embankment, as described below.

Responsibility for the defences along the first part of this defence length lies with NFDC.

2757

At Hurst Castle, there is a 100 m length of 3-6 tonne rock revetment. This revetment and the remainder of this length has been covered with excess shingle obtained from excavations. The existing timber groynes and breastwork have also been covered by the rock and shingle material. There is a masonry castle wall, built in the nineteenth century, to the rear of the defence.

A regular programme of re-nourishment will continue to maintain the spit as an effective barrier protecting the western Solent.

071/1055D

A 1.54km long shingle embankment along Hurst Spit, which was built up with shingle recharge in 1996, see the notes for defence lengths 2757 and 2758.

2758

Immediately to the south of Saltgrass Lane, is a 6-10 tonne rock armoured breakwater, measuring 90 m in a longshore direction, and 50 m in a crosshore direction. The crest of this breakwater is 2.5m ODN.

Over the 1.87 m length south of Saltgrass Lane, the existing shingle embankment has been built up to a crest level of 7m ODN (sloping to 5.0 m ODN at Hurst Castle), and a crest width of 12 m. The crest width prior to this scheme was 5.20 m ODN. The seaward slope of the embankment was built at 1 in 4, with a 1 in 2.5 landward slope.

2759

Under the above scheme, the 550 m length from the eastern rock groyne at Milford to Saltgrass Lane, the existing rock armour was dismantled and re-constructed as a 3-4 tonne rock revetment. The hinterland to this length is rural.

071/1054D See notes for defence length 2759.

2760

The next 250 m to the east, up to Sturt Pond, consists of a concrete stepwork profile backed by a recurved concrete wave wall. At the bottom of the steps is a sloping apron. The concrete construction appears to be in satisfactory condition. The variable beach level means the structure could be in danger of undermining if beach levels reduce significantly. Further protection to this section is afforded by a number of 20 to 30 m long rock groynes constructed over this section. The year of construction of the defence is believed to be 1964.

071/1053D See notes for defence length 2760.

2761

Over the next stretch of 180 m is a concrete wall and stepped apron slab. The apron slab provides adequate space for beach chalets.

Over the entire length between White House and the end of this concrete wall and apron slab, there are timber groynes in a poor state of repair. The year of construction is estimated as 1960.

071/1052D See notes for defence length 2761.

The next 280 m to the east consists of a stepped stone masonry wall constructed in 1964, backed by a wall constructed of concrete blockwork. This rear wall, estimated to have been constructed in 1960, descends from a level of 5.60 m ODN to 5.00 m ODN at its eastern end. To the rear of the landward wall (the concrete blockwork wall) is a promenade and car park. Between the two walls is a 7 m wide lower level promenade which also contains beach chalets. Both these walls are considered to be in a poor condition, requiring maintenance work.

071/1051D See notes for defence length 2762.

The form of construction changes to the east to a 80m length of concrete sea wall backed by a boundary wall, protected by rock armour placed on the beach. The concrete wall is reported to be in a satisfactory condition, whereas the rock armour requires some maintenance. At its eastern end, this wall rises from a level of 5.00m relative to Ordnance Datum Newlyn (mODN) to 5.60m ODN over 10m. The wall was originally constructed in 1939 and renovated in 1992. The rock revetment was constructed in 1994. Due to the relatively low beach and the dependence of the structure on adequate beach levels for stability, this section appears to be vulnerable to undermining.

The eastern side of Milford-on-Sea (from White House to Sturt Pond) is protected by concrete sea walls of slightly varying forms. There is a 170 m length of masonry wall with concrete coping, reported to be in poor condition. The lower part of this wall has a stepped profile. The estimated construction year is 1960.

At Milford-on-Sea over a length of 0.9 km is the weathered Rook Cliff. The cliff toe is protected by a concrete wall founded on a steel sheet piled toe, estimated to have been constructed in 1970. Due to the wall foundations becoming exposed during storms in 1989, 200 m of 2-4 tonne rock revetment and nourishment using gravel rejects was undertaken by NFDC in 1992 ("Hordle Cliff Emergency Works 1992 – Engineer's Report", 1993). At present both the concrete wall and the steel sheet piling is mostly buried under the beach shingle material. The condition of the wall and piling is considered to be satisfactory (only minor maintenance required). There is further protection in the form of timber groynes which are substantially covered by the beach shingle. The groynes are in a poor condition requiring some maintenance work to return them to a satisfactory state.

Between the Beckton Bunny and Milford-on-Sea is the Hordle Cliff. This consists of 2.5 km of unprotected, eroding cliff face over which many significant slippages have been reported. This stretch fronts an area of mainly agricultural land with some residential properties.

2763

2762

2764

2765

3A-11

2766

2767

The outfall at Beckton Bunny consists of a 12" cast iron pipe with concrete surround, contained within steel sheet piles, and behaves in a similar manner to a groyne, in terms of its effect on sediment transport. There is some 2-6 tonne rock armour protection mainly to the eastern side of the outfall. There is heavy algal growth on the rocks and a strong odour from the outfall. It is estimated that the rock armour was originally placed in 1980, with more extensive protection works carried out in March 1996. The cliffs at Beckton are unprotected and are reported to be suffering from significant erosion.

2768

Coast protection measures extend over the 1.88 km length of eroding cliffs in front of New Milton and Barton-on-Sea. Protection takes the form of rock groynes between Cliffhouse Hotel and the Golf Course. The groynes are approximately 50 m long and some of which were constructed between 1975 and 1983, using 4 tonne rock armour. This length is also protected by a 3-4 tonne rock armour revetment which was constructed in 1990. The revetment comprises two parts. The lower part is at beach level, and the higher part protects the upper slope. To the rear of the upper slope is a 7 m wide compacted earth access roadway. Both the rock groynes and the rock revetments are in a satisfactory condition.

2769

Chewton Bunny is on the boundary of NFDC. To the east of this point are significantly eroding cliffs. Naish Farm holiday village is reported to have lost several buildings due to cliff erosion, there is a lack of sediment deposited in this area due to coast protection work west of Highcliffe which intercepts the littoral drift. The length of cliff in front of Naish Farm is unprotected. NFDC were planning to implement a scheme in early 1997 which would have involved depositing 450,000m³ of shingle between Chewton Bunny and Barton-on-Sea. For several reasons NFDC were not able to obtain the material whilst available and the scheme did not proceed.

Responsibility for the defences along this length lies with Christchurch Borough Council.

2601

At Chewton Bunny the 70 m long armour rock, shore-linked, shore-parallel breakwater was constructed in 1991 to protect properties above Chewton Bunny. Cliff drainage was installed in 1993 and shingle was placed in the lee of the breakwater. These measures were reasonably effective in preventing further erosion of the cliffs immediately adjacent to Chewton Bunny by wave action.

2602

At Highcliffe, a timber revetment and groyne scheme was constructed in the 1960s to protect the 1.35km frontage from coastal erosion. A programme of cliff stabilisation works was carried out in the 1970s. The timber groynes were replaced with alternating long and short groynes (70m and 25m long respectively) in 1980, 1984 and 1992. CBC's current policy is to re-nourish the beach. 75,000 tonnes of shingle were placed in 1985, 28,000 tonnes in 1992 and CBC currently place 1-2,000m<sup>3</sup> of nourishment annually at the western end of Highcliffe.

2603

At Steamer Point, a crude 100m long rock revetment was constructed in 1989 to halt terminal erosion.

2604	Immediately to the west a 310m long apron with a massive re-curve
	sea wall was constructed in the 1960s. Although the toe piling is
	currently buried, it is in poor condition and if the beach level falls, the
	piles will deteriorate rapidly.

- A series of six 50m long timber groynes and a concrete revetment with a sheet piled toe were constructed in 1979 to defend 380m length of Friars Cliff. The concrete revetment is deteriorating, with cracks evident and a possible loss of fines immediately behind the sloping upper section of the revetment. The stepped toe of the revetment is currently buried by sand, levels which have increased over the last 10 years.
- At Avon Beach, a further five 50m long timber groynes are backed by a concrete wall, a promenade and a 240m long concrete splash wall. The sand beach has increased in size over the last 10 years.
- Along a further 210m length of Avon Beach, shingle nourishment and two 60m long groynes, constructed from 1 to 4 tonne rock armour in 1988, provide the main defence. The shingle nourishment has been buried by accreted sand. At the rear of the beach there is a large wave wall with a stepped toe, there is a promenade behind the wave wall.
- The primary feature at Gundimore is the 380m long wave wall with a sloping concrete apron and sheet piled toe. Behind the wall a promenade and splash wall provide secondary defences. When the wave wall was constructed in 1978 a large beach accreted and was retained by constructing a series of rubble groynes, using material from the old seawalls. The frontage appears relatively stable.
- Concrete piles were installed around Mudeford Quay in 1935. In 1970 and 1976 sheet piles were installed following the collapse of the concrete piles, further sheet piles were installed in 1946, 1950 and 1961. In early 1994 the piles were at the end of their useful life and a new sheet pile wall was constructed 2m seaward of the existing line of piles. The area between was reclaimed to provide a new quay structure.
- There are no defences protecting the beach huts on this 270m length on the distal end of the Mudeford Sandbank. Currently the beach is deteriorating and the dunes are being lost. CBC consider that there is a need for formal managed defences along this length. (adjust position of CPSE markers on plan, see CBC plan).
- Two 20m long rock groynes and a rock revetment were constructed and shingle re-nourishment was placed on the beach in 1980 to reduce coastal erosion along this 190m length of Mudeford Sandbank. The defences were designed and built to 1970s standards and are now inadequate and need to be upgraded.
- A 200m length of the offshore face of Mudeford Sandbank is protected with a rock armour revetment, three 60 m long rock groynes and shingle re-nourishment completed in 1980. The defences were designed and built to 1970s standards and are now inadequate and need to be upgraded.

2504

A further 270m length on the offshore face of Mudeford Sandbank. Timber and concrete groynes and a seawall were installed in the late 1940s and 1950s. The concrete wall and sheet piled toe were constructed in the 1960s to prevent the breakthrough of the Sandbank. Following this a splash wall was installed to prevent overtopping which was undermining the rear of the wall. In 1991 two rock armour groynes, 60 and 66 m long, were constructed and shingle re-nourishment was placed on the beach. Since 1991 the beach along this length has continued to accrete, the original 12m wide berm of shingle re-nourishment is now covered with sand, and the sheet piled toe is currently buried. The defences here are adequate at present, however beaches are being starved due to updrift deficiencies.

At the Southern end or root of the Sandbank.

2505

At the southern end or root of the Sandbank, four 60m long timber and concrete groynes and a seawall were constructed in the late 1940s and 1950s along a 340m length of the coast to the east of the Long Groyne. The wall was strengthened and rebuilt in parts during 1965 and 1972. In 1985 three timber groynes were replaced and in 1990 the northern groyne was lined with rock armour. The defences along this length are in a poor state of repair, the timber groynes are inadequate, the beach level is low and the old timber revetment is exposed. The Mudeford Sandbank Groyne Scheme is due to start on site in winter 1998/1999 and involves increasing the standard of protection with additional rock groynes and beach recharge.

The following coastal defences are maintained by Bournemouth Borough Council.

2506

On Hengistbury Head a 360m length of coast, immediately to the east of the Long Groyne, a rock revetment, five rock groynes (typically 45m long) and gabions, at the foot of the cliffs, were constructed in 1987 to retain the beach and halt erosion of the cliffs. The groynes have subsequently trapped large volumes of sand, however at the same time the middle of Mudeford Sandbank suffered beach lowering. In 1991 a 20m long rock groyne was added at the northern end of the 1987 groyne scheme to overcome terminal erosion and one of the existing timber groynes was lined with rock armour.

# 5.1.2 Assessment of Defence Standard

Christchurch, Highcliffe, Barton on Sea and Milford on Sea are medium density urban communities which would warrant a standard of protection against the 1 in 100 year storm event. The other lengths of the frontage are protecting agricultural and rural land, or holiday camps, for which a 50 year return period standard of protection would normally be adequate.

Using present day water levels the standard of protection against structural damage was in excess of the 100 year return period event for all structures between Hurst Spit and Christchurch Harbour entrance. Between the Harbour entrance and Hengistbury Head Long Groyne, the standard of protection varies from less than 1 in 1 year to greater than the 1 in 10 year storm event. The agreement with English Nature that enabled the defences to be built in 1985/86 between the Harbour entrance and the Hengistbury Head Long Groyne required a

less than recommended standard of defence to be provided to enable high spring tides to bring sea borne vegetation and seeds to the foot of the cliffs. This was accepted by BBC and the funding authority MAFF.

A similar analysis for the standard after 50 years, allowing for future sea level rise, revealed that the standard of protection against structural damage was in excess of the 100 year return period event for all structures between Hurst Spit and Christchurch Harbour entrance, apart from the tip of Hurst Spit which affords a 20 year return period standard of service. English Heritage are seeking funds to protect Hurst Castle. Between the Harbour entrance and Hengistbury Head Long Groyne, the standard of protection is less than the 1 in1 year event for the entire length.

Christchurch Borough Council (CBC) are in the process of developing a coast protection scheme to improve the standard of defences along Mudeford Sandbank.

Full details of the overtopping and overflow analysis are included in Table 4.1 at the rear of the report.

# 5.2 Christchurch Harbour – (5F-2)

The defence structures in Christchurch Harbour are mainly seawalls. Sandbanks and shingle beaches form the coastline.

# 5.2.1 Description of Defences

- O81/2080 A 30m length of privately owned concrete wall with a pitched toe has a crest level of +1.92m ODN. The wall is in a poor state of repair and is currently being undermined.
- 081/2070 A 70m long sheet steel piled wall retains the garden of a residential block built in the early 1990s. The wall is privately owned and is in a poor state of repair.
- O81/2060 At Mudeford a privately owned 140m long embankment and concrete wall. The wall protects the hotel and its garden and forms a protective face for the embankment.
- 081/2050 A 200m long privately owned wall constructed from timber sheet piles. The wall is in a poor condition since the fill has been washed out from behind the wall.
- O81/2040 The foreshore to the west of Mudeford is protected by a 300m long clay embankment which is in a poor state of repair. The embankment is privately owned. The embankment acts as a protection to a small tidal lagoon and protects the adjacent portion of timber wall.
- This 750m length is defended by a privately owned masonry wall. The condition of the wall is very poor in places. The walls are of varied construction but are generally of a similar height and condition. The shingle beach levels are low and undermine the walls. Some repairs have been carried out at the toe of the walls but erosion is continuing and the stability of the walls is threatened in places.
- 081/2020 A 80m length of privately owned masonry wall, which is in a fair condition.

HALCROW

081/2010 Clay banks and a masonry wall extend over this 100m length.

A 160m long low level gabion wall protects the inshore face of Hengistbury Head and an exposed length of private road that provides access to Mudeford Sandbank. The gabion wall was constructed in 1987 and is in good condition.

The inshore face of Mudeford Sandbank, beach access road and beach huts are protected by a 380m long sandbank which is reinforced in places with a small rock armour revetment. The 30m wide sandbank is subject to gradual erosion. CBC has carried out coast protection duties on Mudeford Sandbank since 1931, under the terms of the lease of the Sandbank from BBC because of the importance in maintaining the Sandbank, to prevent coastal erosion and flooding in Christchurch Harbour. A constant programme of works has been carried out to prevent a breakthrough of the sea through the split and is only now nearing completion.

Overall the attrition on the inshore face of Mudeford Sandbank is threatening the beach huts and the rear of the seaward defences. A new defence strategy is required along this length.

In addition, there are low masonry walls and slipways between Mudeford Quay and the first private properties, protecting the road, car park and some private properties.

# 5.2.2 Assessment of Defence Standard

Christchurch Harbour is a medium density urban community and will warrant protection against a 1 in 100 year return period storm event, in line with MAFF recommendations (PAGN, Annex K).

The standard of defences were assessed using extreme wave height and water level data as discussed in the coastal processes section of the report. Hind-casting analysis provided the wave climate within Christchurch Harbour.

Under present day water levels, seawater will overflow the majority of the structures on the north shore of Christchurch Harbour when the water level is greater than the 1 in 10 year event. Taking account of 50 years of sea level rise, water will also overflow these structures on any event more severe than the 1 in 1 year event.

Structural damage due to overtopping will occur as a result of any storm more severe than the 1 in 5 year and the 1 in 1 year events, for existing and 50 year water levels respectively.

Considering the coastal defences on the inner shore of Mudeford Sandbank, under present day water levels, the defences will provide protection against structural damage during 1 and 20 year storm events, dependant upon the particular length. Taking account of 50 years sea level rise, the defences will provide protection against structural damage during the 1 and 2 year storm events. Overflow calculations provided similar results.

CBC are in the process of developing a scheme on Mudeford Sandbank to improve the standard of the defences. Environment Agency have examined the feasibility of improving protection to the north shore of Christchurch Harbour however there was insufficient economic justification.

Full details of the overtopping and overflow analysis are included in Tables 4.3 at the rear of the report.

# 5.3 Hengistbury Head Long Groyne to Sandbanks Ferry Slipway – (5F-3)

Coastal structures in area 5F-3 range from groynes in conjunction with beach replenishment schemes to the east to groynes backed by seawalls to the west. Sand and shingle beaches form the coastline.

# 5.3.1 Description of Defences

2507

The Hengistbury Head Long Groyne was constructed in 1938 to encourage the accumulation of sediment in front of the cliffs, but this resulted in starving the beaches to the north and an increased rate of slippage of the adjacent cliffs. The mass concrete structure was constructed with dry mix concrete placed inside sand bags along its sides, in 1987 a 20m long groyne with the same armour was added, extending from the middle of its eastern side. The Long Groyne was repaired following the Hurricane in 1988 using rock armour. The landward end of the Long Groyne is protected, whilst the middle third and seaward end are vulnerable to wave attack. Maintenance is not urgent at the moment. The Long Groyne is seen to be a key element in BBC's current coastal management strategy.

2508

On Hengistbury Head at the toe of the cliffs there is currently only a 1.5km long eroding shingle bank. BBC plan to build five 50m long rock groynes to reduce erosion of the cliffs, between Double Dykes and the Long Groyne. Work is programmed to start in October 1998 and is due to finish in spring 1999.

2509

To the east of the BBC's groyne field, the cliffs at Double Dykes continued to erode rapidly, threatening to breach the cliff line to the east. This erosion would have created a flood channel into the southern side of Christchurch Harbour and separated Hengistbury Head from the mainland. To prevent this, in 1986 three 50m long rock groynes and a high gabion wall were constructed to extend the groyne field eastwards and to protect the 370m length of coast. At the same time, the northern end of the flood channel on the southern bank of Christchurch Harbour was protected with gabions. In 1988 143,000 tonnes of shingle were placed to recharge the beach between the Long Groyne and Southbourne promenade. The next recharge is planned for 2003.

2510

In 1987 two 70m long timber groynes were constructed along Solent Beach and a short section of gabion wall was constructed to protect the beach access and low lying cliffs. 143,000 tonnes of beach recharge was placed to recharge the beach between the Long Groyne and Southbourne promenade in 1988. The next phase of beach recharge is programmed for 2003. Two 70m long permeable groynes were constructed along this length in 1976 to reduce the effects of terminal erosion at the end BBC's groyne field. BBC are currently investigating whether to replace the permeable groynes with traditional timber or rock groynes since further groynes have been constructed to the east and there is no longer a terminal erosion problem in this area. The permeable groynes are due to be replaced in 1999.

2511

There are 33 timber groynes along the 4.2km long Southbourne frontage, typically 50m long. For the 52 groynes along their frontage BBC have established a phased replacement programme, maintaining groynes as necessary and replacing them at the end of their 20 to 25 year life. Between 1974 and 1986 approximately two groynes were built per year and from 1986 four to five groynes were built per year. Thus in October 1998 three groynes will be replaced, in 1999 the permeable groynes will be replaced (in defence length 2510) and in 2000 four groynes will be replaced. Therefore the age of the groynes vary between 20 years old and new.

658,000 cubic metres of sand recharge was placed to recharge the beach between Bournemouth Pier and the Southbourne end of the promenade in 1975. Approximately 300,000 cubic metres were placed along this defence length in 1989. The next phase of beach recharge has been programmed for 2003.

Coast protection structures were first constructed in western Poole Bay in the 1890s. Further schemes involved the construction of revetments, seawalls and groynes, progressing eastwards, for example 1907-11 (Bournemouth to Boscombe), 1927-35 (Boscombe to Southbourne) and 1955-75 (Southbourne). By 1975 virtually the whole frontage from Poole Head to Solent Road was protected. Thus the masonry revetments were originally constructed along this frontage between 1927 and 1975, although a short length of vertical masonry wall was constructed in the 1930s. A splash wall was constructed along the entire length in the 1930s.

Boscombe Pier was originally built in 1889 as a 183m long wooden and iron structure. The head was re-built in reinforced concrete in 1927 and the neck in 1960.

2512

Between Boscombe and Bournemouth there are nine timber groynes (typically 50m long), two permeable concrete groynes and one solid concrete groyne (which is an outfall) of varying ages, see note for defence length 2511. The 2.5km masonry revetment was constructed between 1907 and 1911, however only 550m have a steel sheet piled toe. A short length of masonry wall was constructed in the 1930s and a splash wall was constructed in the 1970s, to protect the base of the environmentally sensitive and unstable cliffs.

In 1975 658,000 cubic metres of sand recharge was placed on the beach between Bournemouth Pier and the end of the promenade at Southbourne. The next phase of beach recharge has been programmed for 2003.

A wooden jetty was constructed on the site of Bournemouth Pier in 1861. In 1880 this structure was replaced with a 225m long pier constructed with a lattice girder neck with iron screwpiles. In 1894 and 1909 the pier was extended to 305m. The pier head was rebuilt in 1950, again in 1960 in reinforced concrete and the whole of the promenade deck of the pier was reconstructed in reinforced concrete in 1979/80.

2513

There are ten timber groynes, typically 50m long, of varying age along the 1.9km length of Bournemouth West. The groynes are

maintained and replaced in line with BBC's phased replacement programme. A masonry wall of varying construction extends along the rear of the beach and was constructed between 1909 and 1957. A re-curved wave wall has been built along a short length of revetment to reduce overtopping. To the rear of the promenade a splash wall protects the toe of the cliffs.

As part of the Beach Improvement Scheme Stage 2 carried out in 1974, a dredger dumped 106,260 cubic metres of dredged material between Bournemouth Pier and Durley Chine in the offshore zone where field studies, conducted in conjunction with HR Wallingford, demonstrated that dumped material would be transported onshore due to wave and current action.

Some 300,000 cubic metres of sand recharge was placed on the beach in 1989.

The defences along the following length are maintained by Borough of Poole, unless otherwise stated.

- At Branksome twelve groynes, typically 30m long, defend this 1.3km length of coast. the groynes were constructed in 1980 generally using steel piles and timber planking and are in good condition. The structure at Branksome Chine is a concrete and steel piled outfall. The groynes along this length are not as effective in maintaining the beach since they are short, 30m long, compared to the 50m long groynes along Bournemouth's frontage. At the root of the groynes, the promenade is protected by a stepped concrete wall. Although a short length of seawall was constructed recently, (1985), the majority of the wall was constructed in the 1960s and requires maintenance.
- Along the toe of Canford Cliffs a 130m long near vertical concrete wall was constructed in the 1970s, the crest of which is above promenade level, to protect the cliffs. One 30m long timber groyne was constructed in 1980.
- Along a further 440m length of Canford Cliffs four 30m long timber groynes were constructed in 1980. One or more of these groynes are likely to require major repair within 5 years. At the toe of the cliffs a 440m long concrete wall, with a re-curved crest wall, protects the promenade and cliff toe.
- Further west along Canford Cliffs, one 30m long timber groyne was constructed in the 1970s whilst the remainder of the Groynes were constructed in 1980 whilst the toe of the cliffs and promenade are protected by a 180m long concrete wall with re-curved crest wall and a masonry splash wall.
- The last 450m length of Canford Cliffs are defended by four 30m long timber groynes which were constructed in 1980 and are in good condition. Once again the promenade is protected by a concrete wall. The concrete wall is stepped and was constructed in the 1960s.
- Along this 630m length of Poole Sandbanks, various private properties are protected by a concrete revetment. There are also two low timber groynes. The condition of the revetment varies along its length.

- Along this section of Poole Sandbanks the form of the defences vary with a short length of masonry revetment (100m), near vertical concrete wall (200m) and near vertical concrete wall with wave return wall (160m). The condition of these defences is generally good. The beach is eroding and the remains of a number of rubble groynes constructed in 1898 but removed in the 1990's are being exposed. Borough of Poole are considering how to secure the beach in this area.
- At Poole Sandbanks a 150m length of timber breastwork provides the defence for a further short length (150m) of private properties.
- There are private properties along this 100m length of Poole Sandbanks. "Rock groynes built in 1995/6 have increased beach levels".
- A vertical steel sheet piled wall surmounted by an armour-flex slope was built along this 150m length of Poole Sandbanks to protect the private properties following damage in the 1989/90 storms.

"Rock groynes built in 1995/6 have increased beach levels".

A one to seven tonne rock armour groyne and concrete wall were built in 1990 along this 100m length of Poole Sandbanks to replace damaged groynes.

"Rock groynes built in 1995/6 have increased beach levels".

Vertical sheet steel piles with a concrete capping beam and porous concrete wall were constructed in the 1960s to protect the 200m length of private properties along Poole Sandbanks. The steel piles are in need of replacement. A further length of wall was constructed from masonry in the 1970s during which rock armour was placed at the toe, presumably to prevent undermining. A concrete crest wall was added in 1980 and the beach was re-nourished with 40,000m3 of fine sand in 1992 with material dredged by Poole Harbour Commissioners.

"Rock groynes built in 1995/6 have increased beach levels".

- The defences along this 210m length of Poole Sandbanks were improved in 1990 to defend the Haven Hotel and comprise; a rock revetment, sheet steel toe piling, promenade, concrete re-curved wave wall and a series of steel groynes.
- A 40m long stepped concrete wall was constructed on Poole Sandbanks with sheet steel toe piling to protect the car park adjacent to the ferry crossing and is in good condition.

# 5.3.2 Assessment of Defence Standard

The standard of defences were assessed using extreme height and water level data as detailed in the coastal processes section of the report.

Bournemouth and Poole are medium density urban communities which warrant a 100 year return period standard of protection in line with the Ministry of Agriculture Fisheries and Food (MAFF) Project Appraisal Guidance Notes (PAGN), Annex K.

Hengistbury Head Long Groyne and Double Dykes also warrant a 100 year standard of protection because of their strategic importance in the defence of the coast and protection of properties within Christchurch Harbour.

Using present day water levels the standard of protection against structural damage is in excess of the 100 year return period event for all of the structures in this coastal process unit. Allowing for 50 years of sea level rise, the standard of protection against structural damage is also in excess of the 100 year return period.

Bournemouth Borough Council (BBC) intend to continue monitoring the beach, refurbishing their existing groynes on a rolling programme (which assumes a groyne design life of some 25 years) and predict that the next beach replenishment scheme will be carried out in 2003. The only remaining undefended section of coast along this coastal process unit is between Double Dykes and the Hengistbury Head Long Groyne. BBC are in the process of developing a scheme along this frontage which may involve a series of short armour rock groynes and possibly beach recharge. Borough of Poole are reviewing their defences particularly at the middle section of Poole Sandbanks and are in the process of testing a number of innovative coast defence solutions.

Full details of the overtopping and overflow analysis are included in Table 4.5 at the rear of the report.

# 5.4 Poole Harbour - (5F-4)

# 5.4.1 Description of Defences

The coastal structures in Poole Harbour are predominantly seawalls. Revetments and breakwaters exist at a few locations in the area.

The coastline mainly consists of sandy beaches but mud flats are found within the harbour.

There are various private masonry and concrete walls along this 1.42km length on the inshore face of Poole Sandbanks, whose age and condition varies. The walls have been undermined in places.

The first length is a 300m long privately owned concrete wall on the inshore tip of Poole Sandbanks. The foreshore is littered with the remains of previous walls constructed to prevent the erosion of the high sandbank on which high value property is built and each one is different in height and texture. The quality of the materials used is good, but the design of some of the walls is poor. Generally the walls are in a poor state of repair and BoP plan to provide a rock toe to counteract undermining.

- Along a further 900m length on the inshore face of Poole Sandbanks, a concrete wall was built to protect Sandbanks Road in 1982. There are some signs of undermining. BoP are responsible for the maintenance of this structure.
- At Shore Road a 1.25km concrete wall with bull-nose was constructed in the 1950s, the wall shows signs of significant damage, undermining and cracking. BoP are responsible for the maintenance of this structure. Maintenance work was undertaken in 1995 in order

to prevent collapse. In front of the wall a series of shore/low concrete groynes were constructed in the 1950s. 2418 A 320m length of footpath at Evening Hill is protected by gabions installed in 1975. A number of the gabions have broken and are in need of repair. BOP are progressing a scheme to build a rock revetment along this frontage. 2419 Various masonry and concrete walls defend private properties at Lilliput. There are also some outfalls and jetties along this length. There is a large cast iron outfall pipe running along the back of the foreshore over the last 200m length, and the defences rely heavily on it to prevent undermining. Generally the wall is in poor condition. 2420/2644 Two breakwaters, constructed from tubular steel raking piles and vertical sheet steel piles in 1972/73 provide a sheltered area for the private marina at Lilliput. In addition a 100m long rock revetment constructed at the same time protects the flats built within the marina area. At Salterns Marina, there is a 410m long privately owned breakwater constructed from vertical steel sheet piles and raking tubular steel piles. 2421 A 280m long concrete wall built in the 1930s protects Blue Lagoon. The lagoon is fronted by private properties and a boatyard/pool. Although there are various walls within the lagoon, the PHC wall provides the first line of defence. 2422 A 880m long masonry wall constructed in the 1960s to protect the private properties at Parkstone. This length also includes a marina and boatyards. A new marina breakwater has recently been completed. A concrete faced masonry revetment and 270m long vertical wall 2423 were constructed in the 1930s as reclamation for open space. 2424 A small rock revetment constructed in the 1970s protects a 1.2km length of footpath along the edge of Parkstone Bay. The condition of the revetment is generally good although there is some overtopping damage near the slipway. Part of the formerly undefended length between 2424 and 2425 is now protected by a concrete wall (1994). 2425 Another 160m long small rock revetment constructed in the 1980s defends the coastline at Baiter. The defences along this length will require maintenance. 2426 Immediately to the west a 130m long armour-flex revetment (EA) protects a further length of the coast at Baiter. 2427 The 110m long rubble breakwater at Fishermans Dock protects the coast to the north and provides sheltered moorings for small vessels.

development.

It is proposed to replace the existing breakwater with a 500m long rubble-mound breakwater as part of the proposed boat haven

2428 A short length (150m) of masonry wall constructed in the early 1900's protects the RNLI lifeboat station and car park in Fisherman's Dock. At Poole Quay the construction of the seawall varies along its length. 2429 There is a 570m length of near vertical stone faced concrete wall. constructed in the 1890s. In the 1980s a steel sheet piled wall was installed in front of a 190m length of the older wall. Both walls are protected with timber fenders. PHC maintain these structures. 2430 At Poole Quay a further 190m length of quay wall constructed from concrete. The wall is in a poor state of repair and the remains of timber piles/fenders are visible in front of the wall. PHC maintain these structures. 2431 At West Quay there is a 750m length of sheet steel piled and concrete walls in various states of repair. Private Ownership. 2432 There is a 450m long privately owned small rock revetment on the edge of Holes Bay that protects a number of facilities. The revetment was constructed in the 1980s. 2433 A 50m long concrete wall constructed in the 1990s protects the A350 along the shore of Holes Bay. PBC are responsible for maintaining this structure. 2434 Adjacent to the concrete wall a 2.1km long rock revetment on the east shore of Holes Bay protects the A350 bypass. The level and form of the foreshore varies between saltings and mud/silt. PBC are responsible for maintaining this structure. 2435 A clay embankment was constructed across the middle of Holes Bay in the 1900s. A concrete revetment was added in the 1970s and repairs were carried out in 1993. The structure is owned and maintained by Railtrack and supports the main railway line. Between defence length 2435 and 2436, there are a variety of quay walls and slipways at Cobbs Quay marina, in fair condition generally. The marina has extensive pontoons but no breakwaters, being in a sheltered part of Holes Bay. 2436 At Hamworthy there are 500m of privately owned defences. These generally include concrete walls but also piling towards Poole Bridge. The northern edge of the former power station site has a bituminous revetment. 2437 Sheet steel piling has been installed at New Quay along various lengths between 1924 and 1988. PHC own and maintain the wall and report that it is currently in a variable condition along its length. Poole Harbour Commissioners (PHC) operate the port, which comprises a variety of quay walls (both concrete and steel) of varying ages and one short length of rock revetment. These are maintained regularly by PHC. A 410m long breakwater and rock revetment in Lower Hamworthy 2438 protect the yacht club. Both structures were constructed in 1983,

PHC maintain these structures.

- 2439 At Hamworthy a low eroding bank is the only defence to the railway. There is one outfall structure on the beach. At Hamworthy Park the defences along the 660m length comprise 2440 five 30m long timber groynes and a vertical concrete wall. Parts of the wall have been buttressed and repaired since it was first constructed, probably in the 1920s. However at the eastern end of the wall has been undermined and is in need of repair over a 100m length. BOP recognise that the defences are in need of upgrading, unfortunately the benefit cost ratio is insufficient to justify capital works along this defence length. EA may provide some form of flood protection scheme in future. At Lake a 1.03km length of various masonry and concrete walls 2441 defend a number of private properties. This also includes the marines base and a small marina boatyard. 2442 A short length (90m) of gabion wall, constructed in the 1980s. protects the car park at Lake Pier, to the east of Ham Common. BOP are responsible for the maintenance of this defence length. There is an undefended length in front of Ham common to the east, which is eroding. 2443 At Rockley Sands, to the west of Ham Common, a 150m length of gabion wall was constructed in the 1980s to protect the caravan park. The majority of the wall is in need of repair. 081/1140 No data available. 081/2090 A 60m long privately owned concrete wall on the eastern shore of Brownsea Island. The wall is in poor condition and is at risk of failure due to undermining. 081/2100 A 60m long privately owned wall. Sheet piling encloses the original stone pier, and the whole structure has been capped with a slab which is in good condition. Erosion is a serious problem and rock armour has been placed at the toe of steel sheet piles. 081/2110 A 100m long privately owned masonry wall on the eastern shore of Brownsea Island. The wall is in fair condition, the stonework needs attention, and a rock armour toe has been added recently. 081/2120 A 20m long stone wall which is in good condition, responsibility for maintenance lies with the private owners.
- O81/2130 The shoreline is protected by a 60m length of sandbank and two masonry walls. These defences are in fair condition and are maintained by private owners.
- O81/2140 Along this 240m length on the coast of Brownsea Island there are a series of concrete and timber groynes. The concrete groynes are in a fair condition and perform well whilst the timber groynes are dilapidated and are of little value.

A wall protects the foot of hill. The wall clearly demonstrates its function in protecting the sandhill of Brownsea Island from erosion. From the end of the wall westwards the coastline is a scene of

devastation caused by erosion – fallen trees and unstable cliffs as far as the eye can see.

## 5.4.2 Assessment of Defence Standard

Poole is a medium density urban community which warrants a 100 year return period standard of protection in line with the Ministry of Agriculture Fisheries and Food (MAFF) Project Appraisal Guidance Notes (PAGN), Annex K.

The standard of defences were assessed using extreme wave height and water level data as discussed in the coastal processes section of the report. Hind-casting analysis provided the wave climate within Poole Harbour.

Using present day water levels the standard of protection against structural damage varies along the shore of the Harbour. The standard of protection is greater than 1 in 100 years; on the inshore face of Poole Sandbanks, Parkstone, Poole Quay, Holes Bay, Hamworthy, Lower Hamworthy, Hamworthy Park and Lake Pier. In other areas the standard of protection was much lower, between 1 and 20 years; Sandbanks Road, Blue Lagoon, Parkstone Bay, Baiter, Fisherman's Dock and Holes Bay.

A similar analysis for the standard after 50 years, allowing for future sea level rise, the only areas with a 100 year standard of protection against structural damage were Holes Bay, Hamworthy and Lower Hamworthy. In other areas the standard of protection was lower, in general between 1 and 20 years.

Full details of the overtopping and overflow analysis are included in Table 4.7 at the rear of the report.

## 5.5 South Haven Point to Handfast Point – (5F-5)

The coastal defences in Area 5F-5 are a combination of gabions, sand dunes and clay embankments.

## 5.5.1 Description of Defences

The defences within this coastal process unit are owned and maintained by the National Trust, although the majority of the defences at the southern end of Studland Bay are privately owned.

081/2770 The dunes along this 4.3km length of coast have a typical crest height of +5.0m ODN but do not provide a continuous defence. Gaps between individual dunes occur frequently therefore providing little or defence against flooding. A 160m length of gabions have been placed at the southern end of the dunes.

There is a substantial concrete slipway for the ferry at South Haven Point which acts as groyne.

A major feature and influence is the 19<sup>th</sup> century, training wall which helps to stabilise the northern half of Studland.

081/2780 Immediately to the south of the dunes a 80m long vertical timber seawall with a crest height of +5.4m ODN protects a few timber buildings and a wooded cliff face.

081/2790 There are a mixture of defences along this 100m length, including armour and gabions on the foreshore with clay banks inshore of these defences.

A privately owned 300m length of clay bank on the sand beach 081/2800 foreshore provides a degree of defence, although the 13m high clay and rock cliff face to the rear provides the main coastal defence along this length.

A 100m long 1.0m high privately owned gabion wall provides the only 081/2810 defence to a series of beach huts. Inshore of the beach huts there is a steep wooded cliff face up to +13.0m ODN.

081/2820 Clay banks on the foreshore provide the only protection over a 260m length to a further set of beach huts. Inshore of the huts is a steep wooded cliff face.

#### 5.5.2 Assessment of Defence Standard

There are a series of dunes along the majority of Shell and Studland Bays, although these dunes have a typical crest level of +5.0mODN they do not provide defence against flooding of the heath behind since gaps occur frequently in the dunes. At the southern end of Studland Bay the land rises to cliffs with a typical level of +13mODN. The village of Studland is on this higher ground. Therefore the only structures at risk are temporary timber buildings and beach huts inshore of the beach. This area therefore only warrants defence against a 5 year return period storm event, since there are very few properties at risk from coastal erosion or flooding.

In many areas the toe of the cliffs will still be subject to erosion during extreme storm events, however this would not cause any direct flood damage to any permanent structures. At the southern end of the bay the gabion wall is in a poor state of repair and the beach huts in this area have been moved inland to prevent storm damage.

Full details of the overflow analysis are included in Table 4.9 at the rear of the report.

### Handfast Point to Peveril Point - (5F-6) 5.6

A combination of seawalls and groynes form the coastal defences in Area 5F-6. The foreshore consists of sandy beaches and bedrock.

### 5.6.1 Description of Defences

5000 5 5.57 Along the 30m inshore face of South Haven Point a rubble revetment and masonry wall protect the privately owned Shell Bay boatyard, cafe and the nearby road to the ferry.

> 2302 In North Swanage, four timber groynes, typically 30m long, were constructed along this 240m length in 1962 in an effort to maintain the beach in order to prevent further erosion of the cliffs. The timber groynes appear to be in a reasonable state of repair, although some of the highest planking is missing. The seaward end of the groynes are in the poorest condition. A lot of the sheet piled ends of the groynes have rusted through. The cliffs continue to erode, recently at

Sheps Hollow a section of the cliff slipped destroying the landward end of the most northern groyne.

2303

In North Swanage a number of beach huts and shops on the promenade are protected by a 600m long series of small seawalls, built in the 1920s, of differing construction which follow an erratic line along the toe of the cliffs. The cliffs in this area are unstable and material falls annually onto the promenade. Several attempts have been made to protect the cliffs but groundwater levels and drainage pose a particular problem. In the 1960s the seawall was refurbished, a new concrete and sheet piled toe detail were added and some sections of seawall were rebuilt. Generally, the seawall appears to be in a reasonable state of repair.

A further ten timber groynes, typically 30m long, were constructed in 1962 and appear to be in a reasonable state of repair, although some of the highest planking is missing. The seaward end of the groynes are in the poorest condition and many of the sheet piles have rusted through.

2304

In Swanage the 500m length of coast is defended by a seawall and seven timber groynes, typically 30m long. Generally the seawall is in a good state of repair. Shore Road is immediately behind the seawall and although debris has been thrown up on the road during storms over the last four years, there have been no reports of damage or flooding in this area. The groynes were refurbished in 1985 and a section of seawall toe was rebuilt in recent years. The timber groynes appear to be in a reasonable state of repair, except some of the highest planking is missing and the sheet piled ends of the groynes have rusted through. In 1993 the Outfall Jetty was constructed, seaward of Victoria Avenue, as part of the Swanage Flood Alleviation Scheme.

081/1130

The 1.2km stone wall at the rear of the beach and the timber groynes, see defence codes 2404 and 2405, are in fair condition. Maintenance is the responsibility of PDC.

2305

To the south of Swanage, along this 170m defence length, a foul sewage outfall pipe runs along the foreshore in this area and discharges at Peverill Point. The outfall is owned and maintained by Wessex Water and has a concrete surround which although undermined in places has not degraded since 1993 (when the Coast Protection Survey of England was carried out). A private housing development has been built on a masonry wall which extends along the rear of the foreshore along this defence length. It should be noted that the wall is a boundary wall and not a seawall.

2306

Further east in Swanage Bay, a small 200m long concrete wall protects the houses on a grass bank above. There are two slipways along this defence length and the outfall pipe with concrete surround runs along the foreshore.

## 5.6.2 Assessment of Defence Standard

Swanage Town is a medium density urban community and warrants a 100 year return period standard of protection in line with the Ministry of Agriculture Fisheries and Food (MAFF) Project Appraisal Guidance Notes (PAGN), Annex K.

Using present day water levels, the standard of protection against structural damage along the main section of Swanage Bay is greater that the 100 year event except in the following areas; along the southern half of the seawall between the Mowlem and the Outfall Jetty; the northern half of the seawall between the Ulwell Stream Outfall and the Pines Hotel and north of the Pines Hotel, where the toe of the cliffs are not protected by a seawall.

A similar analysis to assess the standard of defence following 50 years sea level rise revealed that the standard of protection against structural damage was greater than the 5 year event along the main section of Swanage Bay. In addition it was identified that the structures would overflow at the northern and southern ends of the seawall during the 1 in 100 year storm event.

Full details of the overtopping and overflow analysis are included in Table 4.11 at the rear of the report.

## 5.7 Peveril Point to Durlston Head – (5F-7)

## 5.7.1 Assessment of Defences

2307

In Durlston Bay a cliff stabilisation scheme was carried out in 1989 which involved a 7.0m high 60m long armour rock revetment at the cliff toe, facing the 50m high cliffs with rockfill and cliff drainage measures. Cliff erosion was threatening the stability of a block of flats at the top of the cliffs. Erosion was caused by three factors, weathering, groundwater flow and wave action at the toe. The cliff has now been stabilised.

## 5.7.2 Assessment of Defence Standard

The cliff stabilisation scheme, constructed in 1989, will continue to protect this section of the cliffs from erosion. However, the majority of the cliffs along this coastal process unit will be allowed to erode in order to expose the unique geological formations. This length of coast is likely to be designated as a World Heritage Site in the near future, which will protect the geological exposures for future generations.

Full details of the overflow analysis are included in Table 4.13 at the rear of the report.

## 5.8 Assessment of Condition of Foreshore on Defence Structure

Using a combination of three sources of information an attempt has been made to identify those structures which may experience some kind of toe failure as a result of an eroding foreshore.

For each defence length the CPSE (and SDS) data assesses the type of structure and the degree to which the integrity of the structure is dependant upon a high foreshore level. It also makes subjective assessments of the foreshore level as compared with the toe of the structure which it fronts, as well as a judgement of how the foreshore immediately in front of the defence element is changing with

time. When those structures which have a high dependency coincide with a low and/or eroding foreshore, it has been assumed that the structure may experience some kind of toe failure in the future unless some kind of preventative action takes place.

In conjunction with such anecdotal reporting. Halcrow's monitoring software SANDS has been used to establish trends in beach levels.

Detailed analysis was not possible because of the obvious deficiencies in the time series data that is available. A review of SANDS output, some of which is reproduced in Appendix B, highlights obvious often substantial anomalies, such as the elevation and position of permanent features, particularly defence structures, being shown to vary with time. Levels are also frequently inconsistent with those presented under CPSE. Any such observations are commented upon in Tables 4.1 to 4.4. It has had to be assumed for the appraisal that inferred vertical and horizontal control differences at such crests are typical for each profile as a whole. The observations that result from this approach tend to coincide with evidence from the CPSE data assessments though clearly for any detailed appraisal the original data, and any adjustments that might be considered thereto, must be considered with extreme caution.

The locations where the susceptibility of a structure to undermining was appraised were determined by:

- (a) where CPSE (and SDS) identified structures as having a high dependency on beach level for its stability; and/or
- (b) where a typical length of defence had been analysed for overtopping.

The results of the appraisals are given in Tables 4.1 to 4.4 where an undermining risk has been identified or requires future consideration. This is commented upon in the sub-sections below.

5.8.1 Hurst Spit to Hengistbury Head Long Groyne – (5F-1)

Hurst Castle at the end of Hurst Spit has been identified as at risk. Milford-on-sea and Barton-on-sea seawalls and revetments rely on sufficient beach levels and sediment supply to avoid undermining whilst at Highcliffe, nourishment will need to continue to avoid undermining the timber revetment.

5.8.2 Christchurch Harbour – (5F-2)

The foundation levels of some private walls may cause some risk whilst the low level of the gabions on the inside of Hengistbury Head is also unknown.

5.8.3 Hengistbury Head Long Groyne to Sandbanks Fery Slipway – (5F-3)

The Poole and Bournemouth promenades/seawalls rely on beach levels being maintained by large scale nourishment by BBC.

5.8.4 Poole Harbour – (5F-4)

The toe level of some private seawalls is unknown and therefore a risk. Undermining near Sandbanks Ferry is a known existing problem which BOP are considering a scheme for.

## Poole and Christchurch Bay's Shoreline Management Plan : Stage Two

5.8.5 South Haven Point to Handfast Point – (5F-5)

The crude National Trust defences in this area are at risk of undermining due to coastal recession.

5.8.6 Handfast Point to Peveril Point – (5F-6)

The promenade/seawall in front of New Swanage cliffs regularly has its toe piles exposed and therefore undermining is a risk.

5.8.7 Peveril Point to Durlston Head – (5F-7)

No undermining problem is known in this short length.

## **GLOSSARY OF TERMS**

The following terms have been used to describe:

## **Asset Type**

seawall - a shoreline structure whose primary purpose is either to

protect against erosion, or alleviate flooding, or a combination of both, and in which wave action is the dominant design consideration. Quay walls and other vertical walls which have limited exposure to wave action have also

been included within this category.

quaywall - structure with toe below low water, to provide

berthing/unloading facilities for vessels.

embankment - an artificial bank for the most part used in conjunction with

areas of reclamation.

revetment - indicates that the defence consists of or incorporates a facing

treatment involving armour, aprons, pitching or other forms of

revetment treatment.

groynes - groynes or breastwork.

gabions - indicates that rock filled mesh baskets (gabions or

mattresses) have been used to form the defence or prevent

scour.

shore - a natural eroding length of coast with features.

other - any other asset type not otherwise described above,

including breakwaters.

## Structure

The type of component part of a structure is selected from:

armour - random rock or concrete units placed in front of walls or other

man made or natural feature. Type of armour to be recorded

in the database supplementary report.

apron - a layer of rubble stone or concrete slab with or without toe

piles to protect the toe of the sea wall against scour.

bastion - a projecting section of sea wall.

bank - a naturally occurring feature.

breakwater - a rock or concrete armour faced structure which may be

aligned normal or parallel to the coastline. This structure type rather than groyne was to be used when structure extended significantly seaward to low water. Type of structure and materials of construction to be confirmed in the database

supplementary report.

breastwork - vertical or raking timber or steel piled structures supporting

horizontal planking and often with rock infill.

cliff/scarp -	a natural eroding length of coast. For the purposes of the survey, only lengths of coast which were identified as being significantly eroding were to be recorded as part of the database.
beach ridge -	as for cliff/scarp. Used to describe shingle ridges.
marsh fringe -	as for cliff/scarp. Used to describe the eroding seaward limit of marshes.
embankment -	an artificial bank which was likely to incorporate separate revetment protection on its seaward face.
gabions -	mesh baskets with rock filling. Type of mesh material etc to be recorded within the database supplementary report.
groynes -	structures in rock and timber generally perpendicular to the shoreline used to control beach material movement. Description relates to series of groynes which together form the groyne field. Mapping reflects this as a continuous linear feature rather than a series of unconnected features perpendicular to the coast.
piling -	steel, concrete or timber sheet piles (and steel H piles with concrete planks) which form a vertical exposed face. Not used when describing sheet piling to toe of wall or revetment.
toe piling -	as for piling above but relating to sheet piles where used to support the toe of the defence and protect against undermining.
pitching -	a specific form of revetment treatment to the sloping seaward face of a defence or at its toe in which the material described (stone or block) was set in pitch.
recharge -	protection is effected by importation of shingle or sand. Description relates to the lengths of beach which are actively managed using nourishment as recycling of beach material.
revetment -	a cladding of stone, concrete or other material to stabilise and protect shorelines, embankments or shore structures against erosion by wave action or currents. Type of block or concrete unit used to be described in the database supplementary report.
wali -	vertical or battered free standing structure (but not sheet piling) in mass concrete, reinforced concrete, masonry or brickwork.
recurved wall -	as for wall but structure incorporates a substantial recurve feature. A recurve feature is where the top portion of the wall overhangs the main body of the wall, in order to deflect wave energy seaward.
splash wall -	an upstand wall generally set back from the main crest which is used to intercept overtopping water.

## Material

This is the material which best describes the materials of construction of each Defence Element. Where more than one material is present, the major constituent material was used in the database, with the other materials being covered in the supplementary report. Selection was made from the following.

bag - a flexible container made of textiles, plastic or cloth containing sand, rubble or cemented materials as described in the database supplementary report.

block - special regular block units in pre-cast concrete. Examples of such flexible units include "Essex blocks". The upper surface may have been recessed or indented to help dissipate wave energy.

boulder - a worn well rounded rock (diameter generally exceeding 250mm).

clay - natural, fine grained materials, (usually finer than 3mm).

Commonly used in the past to describe materials from which embankments have been constructed.

cobble - a rounded stone (diameter generally 60-250mm).

concrete - used to describe in-situ and large precast structures and smaller scale in-situ revetment treatments.

masonry - a structure using stone or brick materials. Also seawall structures constructed from massive pre-cast concrete blockwork.

mastic - a mixture of finely powered rock and asphaltic material.

rock - uniform lithological composition – more massive than stone.

rubble - rough waste stone, brick or concrete used as wave energy dissipater.

sand - natural beach deposits (0.5 – 4mm in size).

shingle - natural beach deposits usually between 0.7mm and 75mm.

steel - where the main component is made of steel (such as sheet piling).

stone - small fragments or rock. (<600mm in all directions).

timber - where the main component is wood.

## **REFERENCES**

Ministry of Agriculture, Fisheries and Food, (1994). 'Coast Protection Survey of England. Survey Report – Volumes 5.1 to 5.5, Tunbridge Wells Area', Halcrow.

Ministry of Agriculture, Fisheries and Food, (1994), 'Coast Protection Survey of England. Survey Report – Volumes 6.1 to 6.5, Taunton Area', Halcrow.

National Rivers Authority, (1990), 'Sea Defence Survey'.

Hydraulics Research, (1980), 'Design of Seawalls Allowing for Wave Overtopping', Report EX924.

Hydraulics Research, (1993), 'Wave Overtopping of Vertical Walls', Report SR316.

Ministry of Agriculture Fisheries and Food, (1993), 'Project Appraisal Guidance Notes'.

CUR/CIRIA, (1991), 'Manual on the Use of Rock in Coastal and Shoreline Engineering'.

# **TABLES**

					STANDARD OF C	EFENCE TABLE - I	PRESENT		
		L				l <sub>e</sub>		I	
FIOCESS OTHE	Defence Code	Oversow	Vehicles	Overtop	ong Structural Damage	Overall Standard	PAGN Indicative	Location	Comments
5F - 1	571/2757	> 100	N/A	> 1	> 100		Service Level	11	
51 + 1	071/1055	> 100	- 13/0		- 100	> 100	100	Hurst Castle	
	571/2758	> 100	N/A	> 1	> 100	> 100	100	Lb. 1-4 C-14	
	571/2759	> 100	N/A	> 1	> 100 > 100	> 100 > 100	100	Hurst Spit	
	071/1054	> 100	-		- 100	- 100	50 50	Hurst Point	
	571/2760	> 100		<u>.</u>	-	-	100	PATIS C C	
	071/1053	> 100			-			Milford Beach	
	571/2761	> 100	-	·		*	100	ttissad Day (	
	·····					*	100	Milford Beach	
	071/1052	> 100	-	•			100	-	
	571/2762	> 100	•	*			100	Milford White House	
	071/1051	> 100			*	-	100	* :	
	571/2763	> 100	-	-	•	*	100	Milford White House	
	571/2764	> 100	N/A	> 100	> 100	> 100	100	Milford White House	
	571/2765	> 100	N/A	> 100	> 100	> 100	100	Milford Rook Cliff	
	571/2766	> 100	-	*	-	-	50	Hordle Cliff	
	571/2767	> 100	-		-	-	50	Beckton	
	571/2768	> 100	-	•	-	-	100	Barton On Sea	
	571/2769	> 100	-		-		100	Naish	
	681/2601	> 100	N/A	> 100	> 100	> 100	100	Chewton Bunny	
	681/2602	> 100	N/A	> 5	> 100	> 100	100	Highcliffe	
	681/2603	> 100	N/A	> 50	> 100	> 100	50	Steamer Point	
	681/2604	> 100	N/A	> 10	> 100	> 100	100	Steamer Point	
	681/2605	> 100	N/A	> 5	> 100	> 100	100	Friars Cliff	
	681/2606	> 100	> 100	N/A	> 100	> 100	100	Avon Beach	
	681/2607	> 100	> 10	N/A	> 100	> 100	100	Avon Beach	
	681/2608	> 100	-		-	-	100	Gundimore	
	681/2609	<1	<1	N/A	<1	<1	100	Mudeford Quay	
	681/2610	> 100	N/A	<1	>2	>2	20	Christehurch Harbour	
	681/2611	> 100	N/A	<1	<1	<1	100	Mudeford Sandbank	
	681/2503	> 100	N/A	<1	> 1	> 1	100	Mudeford Sandbank	
	681/2504	> 100	N/A	<1	> 50	> 50	100	Mudeford Sandbank	
	681/2505	> 5	N/A	<1	> 1	> 1	100	Mudeford Sandbank	
	681/2506	> 10	N/A	<1	> 5	> 5	50	Hengistbury Head	

Table 4.1a Standard of Defence Table for Process Unit 5F-1

					STANDARD OF	DEFENCE TABLE	FUTURE		
Process Unit	Defence Code	Overflow		Overtop	ping	Overall Standard	PAGN Indicative	Location	Comments
			Vehicles	Pedestrians	Structural Damage		Service Level		
5F - 1	571/2757	> 100	N/A	< 1	> 100	> 20	100	Hurst Castle	
	071/1055	> 100	<b>†</b> -	-	-	-	100	-	
	571/2758	> 100	N/A	<1	> 100	> 100	100	Hurst Spit	
	571/2759	> 100	N/A	< 1	> 100	> 100	50	Hurst Point	
	071/1054	> 100	-	-	-		50		
	571/2760	> 100		-	·	-	100	Milford Beach	
	071/1053	> 100	-	-	*	-	100		
	571/2761	> 100	-	*	_	-	100	Milford Beach	
	071/1052	> 100	-	,	-	-	100	•	
	571/2762	> 100	-	+	-	-	100	Milford White House	·····
	071/1051	> 100	-	,	-	-	100	-	
	571/2763	> 100	-	•	-	•	100	Milford White House	
	571/2764	> 100	N/A	> 100	> 100	> 100	100	Milford White House	
	571/2765	> 100	N/A	> 100	> 100	> 100	100	Milford Rook Cliff	
	571/2766	> 100	-	-	-	-	50	Hordle Cliff	
	571/2767	> 100		-	*	-	50	Beckton	
	571/2768	> 100	,	-	*	<b>"</b>	100	Barton On Sea	
	571/2769	> 100		-	vis.		100	Naish	
	681/2601	> 100	N/A	> 100	> 100	> 100	100	Chewton Bunny	
	681/2602	> 100	N/A	> 1	> 10	> 100	100	Highcliffe	
	681/2603	> 100	N/A	> 5	> 100	> 100	50	Steamer Point	
	681/2604	> 100	N/A	> 1	> 100	> 100	100	Steamer Point	
	681/2605	> 100	N/A	> 1	> 100	> 100	100	Friars Cliff	
	681/2606	> 100	> 10	N/A	> 100	> 100	100	Avon Beach	
	681/2607	> 100	> 5	N/A	> 100	> 100	100	Avon Beach	
	681/2608	> 100	-	-	<u>-</u>	-	100	Gundimore	
	681/2609	<1	<1	N/A	<1	<1	100	Mudeford Quay	
	681/2610	> 100	N/A	<1	<1	<1	20	Christchurch Harbour	
	681/2611	> 10	N/A	<1	<1	<1	100	Mudeford Sandbank	
	681/2503	> 10	N/A	<1	<1	<1	100	Mudeford Sandbank	
	681/2504	> 10	N/A	<1	> 10	> 10	100	Mudeford Sandbank	
	681/2505	< 1	N/A	<1	<1	<1	100	Mudeford Sandbank	
	681/2506	> 2	N/A	<1	>1	>1	50	Hengistbury Head	

Table 4.1b Standard of Defence Table for Process Unit 5F-1

1	~~~					G ASSESSMENT TAB	E		
Process Unit	Defence:Code	Sub Code	CPSEISDS	U Foreshore A	ssessment		NRA Photogrammetry Analys		Comments
5F - 1	571/2757	1	Dependency High	Level Variable	Condition Volatile	Typical Profile Ref.	Lower Foreshore Condition:	Upper Foreshore Condition	
	571/2757 571/2757	3	High High	Veriable Veriable	Votatile Votatile		M		·····
	571/2757	4	High	Variable	Volatile				
	571/2757 571/2757	5 6	High High	Variable Variable	Volatile Volatile	<del> </del>		~~~~~~	
	571/2757	7	High	Variable Low	Volatile Eroding				
	071/1055 571/2758	1	High High	Variable	Volatile				
	571/2758 571/2759	2	High Medium	Variable Low	Volatile Stable				
	571/2759	2	Medium	High	Stable				
	071/1054 071/1054	2	High High	Low Low	Eroding Eroding				
	571/2760 571/2760	1 2	Medium High	Low Low	Volatile Volatile				
	571/2760	3	Medium	Low	Volatile				
	071/1053 071/1053	1 2	High High	Łow Łow	Eroding Eroding				
	071/1053	3	High	Low	Eroding				
	071/1053 071/1053	4 5	High -	Low	Eroding				
	071/1053 571/2761	6 1	- Medium	Low	Eroding				
	571/2761	2	Medium	Low	Eroding				
	571/2761 071/1052	1	High High	Low High	Eroding Eroding				
	071/1052 071/1052	3	High High	High High	Eroding Eroding				
	071/1052	4	•		<u> </u>				
	071/1052 571/2762	<u>5</u>	High Medium	High Low	Eroding				
	571/2762	2	High	Low	Eroding				
	571/2762 071/1051	3	High High	Low Low	Eroding Eroding				
	071/1051 071/1051	2.	High	Low	Erading				
	071/1051	4	High	High	-				
	571/2763 571/2763	2	High High	Varioble Variable	Stable Stable				
	571/2763 571/2764	3	High High	Variable Low	Volatile Volatile				
	571/2764	2	High	Low	Volatile				
	571/2765 571/2765	1 2	Low	Variable Variable	Volatile Volatile				
	571/2765	3	Low	Variable	Volatile Volatile				
	571/2765 571/2765	4 5	High Medium	Variable Variable	Volatile				
	571/2765 571/2765	<u>6</u> 7	Medium Medium	Variable Variable	Volatile Volatile				
	571/2766	1	High	Variable	Volatile				
	571/2767 571/2767	1 2	High High	Variable Variable	Volatile Volatile				
	571/2768	1	High	Veriable	Volatile				
	571/2768 571/2768	3	High High	Variable Variable	Volatile Volatile				
	571/2769 681/2601	1 1	High Medium	Variable Variable	Volatile Stable				
	681/2601	2	Medium	High	Stable				
	681/2602 681/2602	2	High High	Variable Variable	Stable Stable				
	681/2602	3	Medium Medium	Variable Variable	Stable Stable				
	681/2602 681/2602	5	Medium	Variable	Stable				
	681/2603 681/2603	1 2	Medium High	Variable Variable	Volatile Volatile				
	681/2604	1	High	Variable	Volatile				
	681/2604 681/2604	3	High High	Variable Variable	Volatile Volatile				
	681/2605 681/2605	2	High Medium	High High	Stable Stable				
	681/2605	3	High	High	Stable				
	681/2605 681/2606	1	High High	High High	Stable Stable				
	681/2606	2	Medium Medium	High	Stable Stable				
	681/2606 681/2605	4	Medium	High High	Stable				
	681/2607 681/2607	2	High Medium	High High	Stable Stable				
	681/2607	3	Low	High High	Stable Stable				
	681/2608 681/2608	2	High High	High	Steble				
	681/2608 681/2608	3 4	Medium Low	High High	Stable Stable				
	681/2608	5	Low	High	Stable				
	681/2609 681/2609	2	High High	Low Low	Stable Stable				
	681/2609 681/2609	3 4	High High	Low Low	Stable Stable				
	681/2609	5	High	Low	Stable				
	681/2609 681/2609	7	Medium Medium	Łow Low	Stable Stable				
	681/2610	1	Medium	Variable	Eroding				
	681/2611 681/2611	2	Medium Medium	Variable Variable	Volatile Volatile				
	681/2503 681/2503	1 2	Medium Low	Variable Variable	Volatile Volatile				
	681/2504	1	High	High	Accreting				
	681/2504 681/2504	3	High High	High High	Accreting Accreting				
	681/2504	4	Medium	High	Accreting				
	681/2504	<u>5</u>	Law High	High Variable	Stable Volatile				
	581/2505			Variable	Volatile				
	881/2505	2	Medium			1 1			
	681/2505 681/2505 681/2506	2 3 1	Łow Low	Variable High	Volatile Stable				
	681/2505 681/2505 681/2506 681/2506	2 3	Ław	Variable High High	Volatile				
	681/2505 681/2505 681/2506	2 3 1	Low Low	Variable High	Volatile Stable Stable				

Table 4.2 Undermining Assessment Table for Process Unit SF-1

	Defence Code	Overflow		Overtop	ping	Overall Standard	PAGN Indicative	Location	Comments
			Vehicles	Pedestrians	Structural Damage		Service Level		
5F - 2	081/2080	-		-	-	•	100	-	
	081/2070		•	-	-	*	100	-	
	081/2050	,	,			•	100	-	
	081/2050	•	•	-	-	+	100	-	
	081/2040	-	-	-	-	-	100	-	
	081/2030	*	*	-	,		100	-	
	081/2020	-		-	-	-	100	-	
	081/2010	-	-	-	•	-	100		
	681/2501	> 5	<1	N/A	>1	> 1	100	Christchurch Harbour	
	681/2502	> 10	<1	N/A	>20	> 10	100	Christchurch Harbour	
		·········		······································	······································	······································		<u> </u>	

								and the control of th	
Process Unit	Defence Code	Overflow		Overtop	olng	Overall Standard	PAGN Indicative	Location	Comments
			Vehicles	Pedestriane	Structural Damage		Service Level		
5F - 2	081/2080	•	-		-	-	100	-	
	081/2070		•	-	•	*	100	-	
	081/2060	-	-	-	-	-	100	-	
	081/2050	•		-	•	-	100	-	
	081/2040	,	•	•	•	-	100	•	
	081/2030	•	•	٠	•	*	100		
	081/2020	-		-	-	•	100	-	
	081/2010	•	•	-	-	•	100	-	
	681/2501	< 1	<1	N/A	<1	< 1	100	Christchurch Harbour	
	681/2502	> 2	<1	N/A	> 5	> 2	100	Christchurch Harbour	
								***************************************	

Table 4.3 Standard of Defence Table for Process Unit 5F-2

rocess Unit	Defence Code	Sub Code	CP9E/SDS	U Foreshore A	ssessment		NRA Photogrammetry Analys		Comments
			Dependency	Level	Condition	Typical Profile Ref	Lower Foreshore Condition	Upper Foreshore Condition	
5F - 2	081/2080	329	High	Low	Eroding				
	081/2070	328	Medium	Low	Eroding				
	081/2060	327	High	Low	Eroding				
	081/2060	326	High	Low	Eroding				
	081/2050	325	High	High	Accreting				
	081/2046	324	High	High	Stable				
	081/2030	323	High	High	Eroding				
	081/2020	322	High	Low	Eroding				
	081/2010	321	High	Low	Stable			***************************************	
	081/2010	320	High	Low	Stable				
	681/2501	1	High	Low	Stable				
	681/2502	1	Medium	Variable	Votatile				
	681/2502	2	High	Variable	Eroding				

Table 4.4 Undermining Assessment Table for Process Unit 5F-2

					5 I ANDARD OF	DEFENCE TABLE	PRESEN!		
ocess Unit	Defence Code	Overflow		Overtopp	ing	Overall Standard	PAGN Indicative	Location	Comments
	0.00		Vehicles	Petiestrlans	Structural Damage	58.55.50	Service Level		
5F - 3	681/2507	> 50	-	-	÷	-	100	Long Groyne H.Head	
	681/2508	> 100	-	-	-	-	50	Hengistbury Head	
	681/2509	> 100	N/A	<1	> 100	> 100	100	Double Dykes	
	681/2510	> 100	N/A	> 100	> 100	> 100	50	Solent Beach	
	681/2511	> 100	<b>&gt;</b> 1	N/A	> 100	> 100	100	Southbourne	
	681/2512	> 100	< 1	N/A	> 100	> 100	100	Boscome to Bournemouth	
	681/2513	> 100	N/A	< 1	> 100	> 100	100	Bournemouth West	
	681/2401	> 100		~	•	-	100	Branksome	
	681/2402	> 100	N/A	> 10	> 100	> 100	100	Canford Cliffs	······································
	681/2403	> 100	N/A	< 1	> 100	> 100	100	Canford Cliffs	
	681/2404	> 100		-	-	-	100	Canford Cliffs	
~~~~~~~	681/2405	> 100	-	*	-	-	100	Canford Cliffs	
	681/2406	> 100	-		-	*	100	Poole Sandbanks	
	681/2407	> 100	N/A	< 1	> 100	> 100	100	Poole Sandbanks	
	681/2408	> 100	•	*	•	-	100	Poole Sandbanks	
	681/2409	> 100	-	-	•	-	100	Poole Sandbanks	
	681/2410	> 100	N/A	<1	> 100	> 100	100	Poole Sandbanks	
	681/2411	> 100	-			-	100	Poole Sandbanks	
	681/2412	> 100	-	-	-	-	100	Poole Sandbanks	
	681/2413	> 100	-	•		-	100	Poole Sandbanks	
	681/2414	> 100	< 1	N/A	> 100	> 100	100	Poole Sandbanks	

		CE TAE	

Process Unit	Defence Code	Overflow		Overtopp	ing	Overall Standard	PAGN Indicative	Location	Comments
			Vehicles	Pedestrians	Structural Damage		Service Level		
5F - 3	681/2507	< 1	-	-		•	100	Long Groyne H.Head	
	681/2508	> 100	-	,	*	*	50	Hengistbury Head	
	681/2509	> 100	N/A	< 1	> 100	> 100	100	Double Dykes	
	681/2510	> 100	N/A	> 100	> 100	> 100	50	Solent Beach	
	681/2511	> 100	< 1	N/A	> 100	> 100	100	Southbourne	
	681/2512	> 100	< 1	N/A	> 100	> 100	100	Bascome to Bournemouth	
	681/2513	> 100	N/A	< 1	> 50	> 50	100	Sournemouth West	
	681/2401	> 100	•	-	-	<del>-</del>	100	Branksome	
	681/2402	> 100	N/A	< 10	> 100	> 100	100	Canford Cliffs	
	681/2403	> 100	N/A	< 1	> 100	> 100	100	Canford Cliffs	
	681/2404	> 100	-	-	-	-	100	Canford Cliffs	
	681/2405	> 100	-	*	-	•	100	Canford Cliffs	
	681/2406	> 100	-	-	-	-	100	Poole Sandbanks	
	681/2407	> 100	N/A	< 1	> 100	> 100	100	Poole Sandbanks	
	681/2408	> 100	-	-		-	100	Poole Sandbanks	
	681/2409	> 100	-	*	•	-	100	Poole Sandbanks	
	681/2410	> 100	N/A	< 1	> 100	> 100	100	Poole Sandbanks	
	681/2411	> 100	-	-	-	•	100	Poole Sandbanks	
	681/2412	> 100	-	-	-	-	100	Poole Sandbanks	
	681/2413	> 100		•			100	Poole Sandbanks	
	681/2414	> 100	< 1	N/A	> 100	> 100	100	Poole Sandbanks	

Table 4.5 Standard of Defence Table for Process Unit 5F-3

	Detence Code	Sub Code	CPSEF				NRA Photogrammetry Anal		
				Level			Lower Foreshore Condition		
5F - 3	681/2507	11	Medium	Variable	Volatile				
	681/2507 681/2508		Medium	Variable	Volatile				
	681/2508	2	High	Variable Variable	Eroding Eroding				
	681/2509	1	High Low	Variable	Volatile				
	681/2509	2	High	Variable	Volatile				
	681/2509	3	Medium	Variable	Volatile				
	681/2510	1	Medium	Variable	Volatile				
	681/2510	22	Medium	Variable	Volatile				
	681/2510 681/2510	3	Medium	Variable	Volatile				
	681/2510	4	High High	Variable Variable	Volatile Volatile				
	681/2511	1 2	High Medium	Variable	Votatile	<del></del>			
	681/2511	3	Medium	Variable	Volatile				
	681/2511	4	High	Variable	Volatile	***************************************			
	681/2511	5	High	Variable	Volatile				
	681/2511	6	High	Variable	Volatile				
	681/2511	7	Medium	Variable	Volatile				
	681/2511 681/2511	8	Medium	Variable	Volatile				
	681/2511	9	Medium	Variable	Volatile				<del></del>
	681/2511	10 11	Medium Medium	Variable Variable	Volatile Volatile				
	681/2512	1	High	Variable	Volatile				
	681/2512	2	Medium	Variable	Volatile				
	681/2512	3	Medium	Variable	Volatile				
T	681/2512	4	Medium	Variable	Volatile				
	681/2512	5	Medium	Variable	Volatile				ļ
	681/2512 681/2512	6	Medium	Variable Variable	Volatile				<u> </u>
	681/2512	7 8	Medium Medium	Variable Variable	Volatile Volatile	· · · · · · · · · · · · · · · · · · ·			
	681/2512	9	Medium	Variable	Volatile				
	681/2513	1	High	Variable	Volatile				
$\neg \neg$	681/2513	2	High	Variable	Volatile				
	681/2513	3	High	Varlable	Volatile				
	681/2513	4	High	Variable	Volatile				
	681/2513	5	Medium	Variable	Volatile				
	681/2513	6	Medium	Variable	Volatile				<u> </u>
	681/2513 681/2513	7	Medium	Variable	Volatile				
	681/2513	- 8 9	Medium Medium	Variable Variable	Volatile Volatile				
	681/2401	1	High	Low	Eroding			······	
	681/2401	2	High	Low	Eroding				
	681/2401	3	High	Variable	Volatile				
	681/2401	4	Medium	Low	Eroding				
	681/2402	1	High	Variable	Votatile				
	681/2402 681/2403	2	Medium	Variable	Votatile				
	681/2403	1	Medium :	Variable Variable	Eroding Volatile				
	681/2404	2 1	Medium High	Variable	Eroding				
	681/2404	2	High	Variable	Volatile				<u> </u>
	681/2404	3	High	Variable	Votalile				
	681/2405	i	High	High	Stable				
	681/2405	2	Medium	High	Stable				
	681/2406	1	High	Variable	Volatile				
	681/2407 681/2407	1	High	Variable	Eroding				<u> </u>
	681/2407	2	High High	Variable Variable	Eroding Eroding				
	681/2408	1	High	High	Stable		***************************************		
	681/2408	2	High	High	Stable				
	681/2408	3	High	High	Stable				
	681/2409	2	High	High	Stable				
	681/2409	3	High	High	Stable				
	681/2410 681/2410	1	High	High	Stable				
	681/2410	<u>3</u>	High High	High High	Stable Stable				
+	681/2411	1	Medium	Variable	Stable			****	
	681/2411	3	High	Variable	Stable			***************************************	
	681/2411	4	High	Variable	Stable				
	681/2412	1	High	High	Stable		~~~		
	681/2412	2	High	Low	Eroding				
	681/2412 681/2412	3	High	Low	Eroding				
	681/2412 681/2412	4	High	Low	Eroding				
	681/2412	5 6	High Low	Łow Variable	Eroding Stable				
	681/2412	7	Low Medium	Variable Variable	Volatile			<del></del>	
	681/2412	8	High	Low	Eroding				
	681/2412	9	High	Variable	Stable				
	681/2412	10	High	High	Stable				
	681/2413	1	Low	Variable	Stable				
	681/2413	2	Medium	Variable	Stable				
	681/2413	3	High	Variable	Stable				
1	681/2413	4	High	Variable	Slable				
+	681/2414	1	Medium	Low	Eroding				

Table 4.6 Undermining Assessment Table for Process Unit 5F-3

ess unit	Defence Gode	Overflow	4	Overtoppin	9	Overall Standard	PAGN Indicative	Location	Comments
Control of the Contro			Vehicles	Pedestrians	Structural Damage	0.00	Service Level		Volumenta
5F - 4	681/2415	> 100	[ -	-	-	-	100	Poole Sandbanks	
	081/2150	> 100	-		,	-	100		
	081/1120		-			-	100	· <del> </del>	
	681/2416	> 5	N/A	< 1	> 5	> 5	100	Sandbanks Road	
	681/2417	> 100	N/A	< 1	> 100	> 100	100	Shore Road	<del> </del>
	081/2180	> 100	-	~	-	*	100	-	
	081/2170	> 100	-	-	-	*	100	<del>                                     </del>	<del> </del>
	081/2160	> 100	-	-	-	*	100	<del></del>	·
***************************************	681/2418	> 2	-	-		-	100	Evening Hill	<del></del>
***************************************	081/1080	> 2	1 -	-	-	*	100	- vetting this	<u> </u>
	681/2419	> 100	1	-	-		100	Lilliput	
	081/2210	> 100	-	-	-		100	Limput	
	081/2200	> 100		-	-	-	100	<del> </del>	<del></del>
	081/2331	-		-			100	<u> </u>	
	081/2270	> 100		-	-		100	<u> </u>	<del> </del>
	081/2280		-	-	-		100	<u> </u>	<u> </u>
	681/2420	> 100		-	-			-	<u> </u>
	681/2444	> 100				-	100	Lilliput	<u> </u>
	081/2300						100	Lilliput	
	081/2260			~~~~			100		
	081/2250		-	*	•		100		
	081/2240	-	-		*		100	-	
	681/2421	> 2	·				100	<u> </u>	
	081/2421	> %	N/A	< 1	> 2	> 2	100	Blue Lagoon	
			*		*	-	100	<u>-</u>	
	081/2220	-	-	*		-	100		
	081/2330			-		-	100	•	
	081/2320	-	-	-			100	-	
	681/2422	> 100	N/A	< 1	> 100	> 100	100	Parkstone	
	681/2423	> 100				-	5	Parkstone Bay	<u> </u>
	081/1070			-	*	-	5	^	
	081/1060	~		-	*	-	100	*	
	681/2424	> 100	N/A	< 1	> 20	> 20	5	Parkstone Bay	
	681/2425	< 1	N/A	< 1	<1	< 1	50	Baiter	
	681/2426	< 1		-	*	-	100	Baiter	<u> </u>
	681/2427	< 1		-	•	-	100	Fishermans Dock	
	081/2430		-	-	•	-	100	*	
	081/2420	-	-	-		-	100		
	081/2410	-	-	-		-	100	*	<del> </del>
	081/2400	-		-		-	100	-	
	081/2390	-	-	-			100	-	
	081/2380	-		-		-	100	-	
	681/2428	> 1	N/A	< 1	> 1	>1			<del> </del>
	681/2429	» 100		-				Fishermans Dock Poole Quay	
	681/2430	> 100	N/A	< 1	> 100	> 100			
	081/2370	-					100	Poole Quay	
	081/2360	-		-					
	081/2350						100		
	681/2431	> 2	-:				100	-	
	081/2340			*				West Quay	
	081/2530			•			100	-	
					<u>-</u>		100	-	
	081/2520		·	*		· ·	100	-	
	081/2510			*			100	-	
	081/2500			-		4	100	-	
	081/2490				<u> </u>	-	100	*	
	081/2480	-				-	100	*	
	081/2470	-	-	-			100	*	*****
	681/2432	> 20		-		-	100	Holes Bay	
	081/2460	-	-	-	- 1	~	100		
	081/2450	-	-	-	*	*	100	<u>-</u>	
	081/2440	-	-	*	-		5		
T	681/2433	> 2	<1	N/A	> 1	>1		Holes Bay	
	681/2434	> 100	N/A	< 1	> 100	> 100		Holes Bay	
	081/1050	-	-	-		- 100	5	notes Bay	
	681/2435	> 100	< 1	N/A	> 100	> 100			
	681/2436	> 100	N/A	> 5	> 100	> 100		Holes Bay	
	681/2437	> 100			- 100	2 100		damworthy	
	681/2438	> 100	N/A	> 20	> 100	·····		Vew Quay	·
	681/2440	> 100	N/A	< 1		> 100		ower Hamworthy	
	681/2441	> 100			> 100	> 100		lamworthy Park	
	681/2442	> 100	- N/A					.ake	
			N/A	>1	> 100	> 100		ake Pier	
	681/2443	>1		•		-		Rockley Sands	
	081/1140	-				-	5	-	
	081/2090	-		-	-		100	-	
	081/2110	-	-	-	-		100	-	
	081/2120	-	-		-	****	100	-	
T	081/2130	-	-	-	-	-	100		
~~~~	081/2140					1		-	

Table 4.7a Standard of DefenceTable for Process Unit 5F-4

ocess Unit	Defence Code	Overflow		Overtoppin	g	Overall Standard	PAGN Indicative	Location	Comments
			Vehicles		Structural Damage	07-15-10-10-10	Service Level	Coalion	Commence
- 4	681/2415	> 100	*		-		100	Poole Sandbanks	
	081/2150	·	*	-	-		100	-	
	081/1120			-	-		100	-	
	581/2416	<1	N/A	< 1	< 5	< 5	100	Sandbanks Road	
	681/2417	> 20	N/A	< 1	> 10	> 10	100	Shore Road	
	081/2180	-		-	-	*	100		
	081/2170 081/2160			-	*		100	-	
	681/2418		-	-	-	· ·	100	•	
	081/1080	< 1	*	- :	-	-	100	Evening Hill	ļ
	681/2419	ļ				•	100		
	081/2210	> 100			-		100	Lilliput	
	081/2200	·					100		
	081/2331		*		-		100		
	081/2270	-				-	100		
	081/2280	-	-			h	100		
	681/2420	> 100				-	100	Lilliput	<del></del>
	681/2444	> 100	*	*	*		100	Lilliput	
	081/2300	-	-	*	-		100	-	
	081/2260	-	-	-	-	-	100	-	
	081/2250	-			-	-	100		
-	081/2240		*	*	*	-	100	-	
	681/2421	< 1	N/A	<1	< 1	< 1	100	Blue Lagoon	
	081/2230	-	-	-	-	. н	100	-	
	081/2220	*	*	-	*	-	100	+	
	081/2330	-	-	-	-	-	100	-	
	081/2320	*	h	-	-		100	-	
	681/2422	> 20	N/A	< 1	> 10	> 10	100	Parkstone	
	681/2423	> 100			"	-	5	Parkstone Bay	
	081/1070	μ.	٠	*	*	-	5		
	081/1060	-	+	•	-		100	٠	
	681/2424	> 20	N/A	<1	> 5	> 5	5	Parkstone Bay	
	681/2425	< 1	N/A	< 1	< 1	< 1	50	Baiter	
	681/2426	< 1	<u>-</u>		<u> </u>	*	100	Baiter	
	681/2427	<1	-			<u>-</u>	100	Fishermans Dock	
	081/2430	-	-	-	-	-	100	•	
	081/2420	-		-	-	-	100	-	
	081/2410	-		_		*	100	-	
	081/2400	-	*		*		100	-	
	081/2390	٠.	-	•			100	+	
	081/2380		-	-	-	-	100	-	
	681/2428 681/2429	< 1	N/A	<b>&lt;1</b>	<1	<1		Fishermans Dock	
	681/2429	> 5		**	-	•	100	Poole Quay	
	081/2370	> 5	N/A	<1	> 5	> 5		Poole Quay	
	081/2360			*	•	٠	100	<u> </u>	
	081/2350	-	-	······································	-		100		
	681/2431						100		
	081/2340	<1			-			West Quay	
	081/2530			-		*	100	*	
	081/2520		<del>-</del>		-		100		
	081/2510			-			100		
	081/2500				- :		100	-	
	081/2490					-	100	-	
	081/2480					-	100		
	081/2470			P			100		
	681/2432	> 1		-			100	Holes Bay	
	081/2460			-			100	noles bay	
	081/2450			*	*	-	100	-	
	081/2440						5		
	681/2433	< 1	N/A	<1	< 1	<1		Holes Bay	
	681/2434	> 20	N/A	< 1	> 20	> 20		Holes Bay	
	081/1050	*	*	-	-	P	5	-	
	681/2435	> 100	< 1	N/A	> 100	> 100	~~~~~~	Holes Bay	
	681/2436	> 100	N/A	<1	> 100	> 100		Hamworthy	
	681/2437	> 100		-				New Quay	
	681/2438	> 100	N/A	> 2	> 100	> 100	100	Lower Hamworthy	
	681/2440	> 20	N/A	<1	> 20	> 20	5	Hamworthy Park	
	681/2441	> 100			-	-	100	Lake	
	681/2442	> 50	< 1	N/A	> 50	> 50	5	Lake Pier	
	681/2443	< 1	-		-		100	Rockley Sands	
	081/1140	-		-	-	-	5		
	081/2090	+				-	100	-	
	081/2110	-	· ·	•	*	-	100	-	
	081/2120	-		-		-	100		
	081/2130			*	-	<u>.</u>	100	,	

Table 4.7b Standard of DefenceTable for Process Unit 5F-4

Coast Unit   Defence Coast	ince Code	Sub Code		***********					
5F. 4 681/2415			CPSESUS	U Foreshore A	95038ment		NRA Photogrammetry An	slysia	
081/2150 081/1120 081/1120 081/1120 681/2416 681/2417 681/2417 081/2180 081/2170 081/2170 081/2170 081/2170 081/2170 081/2170 081/2210 081/2200 081/2200 081/2200 081/2270 081/2230 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2330		100	Dependency	Level	Condition	Typical Profile Ref		Upper Foreshore Condition	Comments
081/2150 081/1120 081/1120 081/1120 681/2416 681/2417 681/2417 081/2180 081/2170 081/2170 081/2170 081/2170 081/2170 081/2170 081/2210 081/2200 081/2200 081/2200 081/2270 081/2230 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2330	81/2415	1	High	Low	Eroding	At a same a second	and the broken with the state of the water to be a second	County Colesions Countries	
081/1420 081/1420 081/1420 681/2416 681/2417 681/2417 081/2180 081/2170 081/2170 081/2170 081/2180 081/2170 081/2180 081/2210 081/2200 081/2200 081/2200 081/2200 081/2200 081/2300 081/2240 081/2250 081/2240 081/2240 081/2240 081/2240 081/2240 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2300		339	High	Low	Eroding			<del> </del>	ļ
081/1120 681/2416 681/2417 681/2417 681/2417 081/2180 081/2170 081/2170 081/2170 081/2160 681/2418 081/2418 081/2180 081/2210 081/2200 081/2200 081/2270 081/2270 081/2270 081/2270 081/2270 081/2270 081/2270 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2330		218	Low	Low	Stable		<del> </del>	<u> </u>	
681/2416 681/2417 681/2417 681/2417 681/2418 681/2417 681/2180 681/2170 681/2170 681/2170 681/2180 681/2418 681/2418 681/2418 681/2418 681/2200 681/2200 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2270 681/2200 681/2250 681/2240 681/2420 681/2420 681/2421 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2400 681/2400 681/2400 681/2400 681/2400 681/2400 681/2400 681/2400 681/2400 681/2400 681/2400 681/2400		219	Low	Low	Stable		<del> </del>		<u> </u>
681/2417 681/2417 681/2417 681/2180 681/2180 681/2170 681/2170 681/2160 681/2160 681/2160 681/2418 681/2418 681/2418 681/2210 681/2200 681/2270 681/2270 681/2270 681/2270 681/2270 681/2280 681/2420 681/2420 681/2420 681/2420 681/2420 681/2420 681/2250 681/2250 681/2250 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2220 681/2220 681/2230 681/2230 681/2230 681/2230 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2240 681/2230 681/2200 681/2230 681/2240 681/2423		1	High	Variable	Valatite			<u> </u>	
681/2417 081/2180 081/2180 081/2170 081/2170 081/2170 081/2170 081/2180 681/2418 081/1080 681/2419 081/2200 081/2200 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2330 081/2330 081/2330 081/2330 081/2330 081/2444 081/2240 681/2421 081/2240 681/2421 081/2230 081/2230 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2300 081/2000		1	<del></del>	Variable					<u> </u>
081/2180 081/2180 081/2170 081/2170 081/2170 081/2170 081/2180 681/2418 081/1080 681/2419 081/2200 081/2200 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2330 081/2330 081/2330 081/2330 081/2330 081/2340 081/2441 081/2441 081/2240 681/2421 081/2240 081/2240 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2300		2	High		Volatile				
081/2180 081/2170 081/2170 081/2170 081/2170 081/2160 681/2418 081/1080 681/2210 081/2200 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2300	····	<b></b>	Medium	Low	Volatile		<u> </u>		
081/2170 081/2170 081/2170 081/2170 081/2180 681/2418 081/1080 681/2210 081/2200 081/2200 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2240 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2330 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300 081/2300		344	High	High	Stable				
081/2170 081/2180 681/2418 081/1080 681/2419 081/2200 081/2200 081/2270 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2330 081/2330 081/2330 081/2330 081/2421 081/2421 081/2230 081/2240 681/2423		343	High	Low .	Stable		ļ	<u> </u>	
081/2160 681/2418 081/1080 681/2419 081/2210 081/2200 081/2270 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2220 081/2230 081/2300 081/2300 081/2300 081/2401 681/2421 681/2421 681/2421 681/2423 681/1080 081/1080 081/1080		342	High	Low	Stable				
681/2418 081/1080 681/2210 081/2200 081/2270 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2330 081/2330 081/2330 081/2330 081/2330 081/2300 081/2000		341	High	Low	Stable				
081/1080 081/1080 081/1080 081/1080 081/1080 081/1080 081/1080 081/1080 081/1080		340	High	Low	Stable				
681/2419  081/2210  081/2200  081/2231  081/2270  081/2270  081/2280  681/2420  681/2420  681/2444  081/2300  081/2300  081/2300  081/2300  081/2250  081/2250  081/2250  081/2250  081/2240  681/2421  081/2230  081/2230  081/2230  081/2230  081/2230  081/2240  681/2421  681/2423		1	High	Variable	Volatile	······································			
084/2210 084/2200 084/2200 084/2270 084/2270 084/2270 084/2280 684/2420 684/2420 684/2420 084/2300 084/2300 084/2300 084/2300 084/2250 084/2250 084/2250 084/2250 084/2250 084/2250 084/2220 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2230 084/2330 084/2423 084/4079 084/4080 084/4080 084/4080 084/4080	31/1080	215	Medium	High	Stable				
081/2200 081/2270 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2444 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2240 681/2421 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2240 681/2421 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 081/1070 081/1080 081/1080 081/1080	31/2419	1	High	Variable	Volatile				
081/2331 081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2444 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2240 681/2421 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 081/1070 081/1080 081/1080 081/1080	31/2210	347	High	Low	Stable				
081/2270 081/2270 081/2270 081/2280 681/2420 681/2420 681/2444 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2230 081/2230 081/2240 681/2421 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 681/2423 081/1070 081/1080 081/1080 081/1080	1/2200	346	High	Low	Stable				
081/2270 081/2280 681/2420 681/2420 681/2444 081/2300 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2230 081/2330 081/2320 681/2422 681/2423 681/2423 681/2423 681/2423 681/2423 081/1070 081/1080 081/1080 081/1080	1/2331	-	~						
081/2280 681/2420 681/2420 681/2420 681/2420 081/2300 081/2300 081/2300 081/2300 081/2260 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2220 081/2330 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1080 081/1080 081/1080	1/2270	357	Low	Low	Stable			<b></b>	
681/2420 681/2420 681/2444 081/2300 081/2300 081/2300 081/2300 081/2250 081/2250 081/2250 081/2240 681/2421 081/2230 081/2230 081/2230 081/2220 081/2220 681/2422 681/2422 681/2423 681/2423 081/2400 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200 081/200	1/2270	358	Low	Low	Stable				
681/2420 681/2444 081/2300 081/2300 081/2300 081/2300 081/2300 081/2260 081/2250 081/2250 081/2240 081/2240 681/2421 081/2230 081/2230 081/2220 081/2330 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060	1/2280	359	Low	Low	Stable				
681/2444  081/2300  081/2300  081/2300  081/2300  081/2260  081/2250  081/2250  081/2240  081/2240  081/2220  081/2220  081/2220  081/2330  081/2330  081/2320  681/2422  681/2422  681/2423  681/2423  081/1070  081/1060  081/1060  081/1060	1/2420	1	High	Low	Votatile				
681/2444  081/2300  081/2300  081/2300  081/2300  081/2260  081/2250  081/2250  081/2240  081/2240  081/2220  081/2220  081/2220  081/2330  081/2320  681/2422  681/2422  681/2423  681/2423  081/200  081/1000  081/1000  081/1000  081/1000		2	Medium	Variable	Volatile				
081/2300 081/2300 081/2300 081/2300 081/2300 081/2260 081/2250 081/2250 081/2240 081/2240 081/2240 081/2230 081/2230 081/2220 081/2330 081/2320 681/2422 681/2422 681/2423 081/2403 081/1070 081/1060 081/1060 081/1060		1	High	Low	Volatile	···			
081/2300 081/2300 081/2300 081/2300 081/2260 081/2250 081/2240 081/2240 081/2240 081/2240 081/2230 081/2230 081/2220 081/2220 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060		361	Low	Low	Stable	<del></del>			
081/2300 081/2260 081/2260 081/2250 081/2240 081/2240 081/2240 081/2240 081/2230 081/2230 081/2230 081/2230 081/2220 081/2220 081/2320 681/2422 681/2422 681/2423 081/1070 081/1070 081/1060 081/1060 081/1060 081/1060		362							
081/2260 084/2250 084/2250 084/2240 084/2240 084/2240 084/2240 084/2230 084/2230 084/2230 084/2220 084/2220 084/2330 081/2320 681/2422 681/2423 681/2423 081/1070 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060			High	Low	Stable				
081/2250 081/2250 081/2240 081/2240 081/2240 081/2230 081/2230 081/2230 081/2230 081/2230 081/2220 081/2220 081/2220 081/2320 681/2422 681/2422 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060		363	High	Low	Stable				
081/2250 081/2240 081/2240 681/2241 081/2230 081/2230 081/2230 081/2220 081/2220 081/2220 081/2330 081/2320 681/2422 681/2422 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060		356	Low	Low	Stable				
081/2240 081/2240 681/2421 081/2230 081/2230 081/2230 081/2220 081/2220 081/2330 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060 081/1060	——	355	Low	Low	Stable				
081/2240 681/2421 081/2230 081/2230 081/2220 081/2220 081/2330 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060		354	Low	Low	Stable	·			
681/2421  081/2230  081/2230  081/2220  081/2220  081/2330  081/2320  681/2422  681/2422  681/2423  681/2423  081/1070  081/1060  081/1060  081/1060  081/1060  081/1060		353	High	Low	Stable				
081/2230 081/2230 081/2220 081/2220 081/2230 081/2330 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2240	352	High	Low	Stable				
081/2230 081/2220 081/2220 081/2330 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2421	1	High	Variable	Volatile				
081/2220 081/2220 081/2330 081/2320 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2230	351	High	High	Stable				
081/2220 081/2330 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2230	350	High	High	Stable				
081/2330 081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2220	349	High	High	Stable				
081/2320 681/2422 681/2422 681/2423 681/2423 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060 081/1060	1/2220	348	High	High	Stable				·····
681/2422 681/2423 681/2423 081/1070 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2330	366	High	Low	Stable				
681/2422 681/2423 681/2423 081/1070 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2320	365	High	Low	Stable				
681/2423 681/2423 081/1070 081/1070 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2422	1	High	Variable	Votatile				
681/2423 681/2423 081/1070 081/1070 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060	1/2422	ż	Low	Low	Stable				
681/2423 081/1079 081/1070 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060		1	Medium	Low	Stable				
081/1070 081/1070 081/1060 081/1060 081/1060 081/1060 081/1060		2	Medium	Low	Stable				
081/1070 081/1080 081/1080 081/1080 081/1080 081/1080		213	Medium	High	Stable				·
081/1060 081/1060 081/1060 081/1060 081/1060		214							
081/1060 081/1060 081/1060 081/1060			Low	High	Stable				
081/1060 081/1060 081/1060 081/1060		207	Low	Low	Stable				
081/1060 081/1060 081/1060		208	Low	High	Stable				
081/1060 081/1060		209	Medium	High	Stable				
081/1060	——— <del>-</del>	210	Medium	High	Stable				
		211	Medium	High	Stable				
081/1060	/1060	212	Medium	High	Stable				
	/1060	443	-	- [					
681/2424	/2424	1	High	Variable	Volatile	7			
681/2425	/2425	1	Low	Variable	Volatile				
681/2426	/2426	1	High	High	Stable .				
681/2427	/2427	1	High	Low	Volatile				
081/2430	/2430	379	High	Low	Stable			******	
081/2430		378	Low	Low	Stable	<del></del>			

Table 4.8a Undermining Assessment Table for Processing Unit 5F-4

			- restriction	J Foreshore A			NRA Photogrammetry Ana	hele	
Init	Defence Code	Sup Code		Level	Condition		Carlot and Carlot and American Street, and the Carlot and Carlot a	Upper Foreshore Condition	Comments
	081/2410	375	Dependency Low	Low	Stable	Typical Profile Ref			
-	081/2410	374	Low	Low	Stable				<b></b>
-	081/2400	373	Low	Low	Stable				
	081/2390	372	Low	Low	Stable				
ᅱ	081/2380	371	Low	Low	-				
	681/2428	1	High	Low	Stable				
┪	681/2429	1	High	Low	Stable				
$\dashv$	681/2429	2	High	Low	Stable				
-	681/2430	1	High	Low	Stable				<u> </u>
1	081/2370	370	Low	Low					<u> </u>
1	081/2360	369	Low	Low					<del></del>
┪	081/2350	368	Low	l.ow					
+	681/2431	1	High	Low	Stable	<del> </del>			<u> </u>
┥	081/2340	367	Low	Low					<del> </del>
┪	081/2530	390	High	Low	Stable			<b> </b>	<del> </del>
┥	081/2520	389	Low	Low	Stable				
-	081/2510	388	High	Low	Stable				
+	081/2500	387	Low	Low	Stable				
-	081/2300	386	High	Low	Stable				<u> </u>
$\dashv$	081/2480	-385	Low	Low	Stable				<del> </del>
-	081/2470	384	High	Low	Stable				
	681/2432	1	Low	High	Stable				
-	081/2460	383	Low	Low	Stable				
-	081/2450	382	High	Low	Stable				
-	081/2450	381	Low	Low	Stable				
+	081/2440			-	- C(ADIC				
$\dashv$	681/2433	1		Low	Stable				-
-		1	High Low	Variable	Stable				
4	681/2434	206	Low	High	Stable				
+	081/1050 681/2435	1	High	Variable	Stable	***************************************	······		<del> </del>
+	681/2435	2	High	Variable	Stable				
+	681/2436	1	High	Low	Stable				
+	681/2437	1	High	Low	Stable				
+	681/2437	2	High	Low	Stable				
$\dashv$	681/2437	3		Low	Stable				
+	681/2437	4	High High	Low	Stable				
+	681/2437	5	High	Low	Stable				
+	681/2438	1	Medium	Low	Stable	······			<u></u>
+	681/2438	2	Medium	Low	Stable				<del> </del>
+	681/2439	1	High	Variable	Eroding				
+	681/2439	1	High	Low	Volatile				<del> </del>
+	681/2440	2	Medium	Variable	Volatile				<u> </u>
+	681/2441	1	High	Variable	Volatile				
+	681/2442	1	High	Variable	Volatile				
+	681/2442	1	High	Variable	Volatile				
+	681/2443	2		Variable Variable	Volatile			***************************************	
+		222	High	High	Eroding	·····			
+	081/1140	330	High High	Low	Eroding				<del> </del>
4	081/2090							<u> </u>	<b></b>
+	081/2110	332	Low	Low	Stable				<b> </b>
-	081/2120	333	Low	Low	Stable				
4	081/2130	334	High	Low	Slable				ļ
4	081/2130	335	High	High	Stable				
4	081/2140	336	High	Low	Stable				ļ
4	081/2140	337 .	High	Low	Stable				ļ
-	081/2140	338	High	Low	Stable			-	1

Table 4.8b Undermining Assessment Table for Processing Unit 5F-4

				ST	ANDARD OF DEFEN	CE TABLE - PRESE	NT		
Process Unit	Defence Code	Overflow		Overtop	ping	Overall Standard	PAGN Indicative	Location	Comments
			Vehicles	Pedestrians	Structural Damage		Service Level		
5F-5	081/2770	< 1	-	*		-	5	-	
	081/2780	> 100	-	-	-	-	20		
	081/2790	-	-	-	,	-	20	-	
	081/2800	> 100	-	-		-	50	-	
	081/2810	> 100	-	+	-	-	50	•	
	081/2820	-	-	*	~	-	50	-	
					STANDARD OF	DEFENCE TABLE	- FUTURE		
Process Unit	Defence Code	Overflow			STANDARD OF	DEFENCE TABLE	-FUTURE		
Process Unit	Defence Corle	Overflow		Overtop		DEFENCE TABLE  Overall Standard	- FUTURE PAGN Inditative Service Level	Location	Comments
Process Unit	Defence Code-	Overflow < 1		Overtop	ping:	DEFENCE TABLE  Overall Standard	-FUTURE PAGN Indicative		
Process: Unit			Vehicles	Overtop Pedestrians	ping:	DEFENCE TABLE  Overall Standard	- FUTURE PAGN Indicative Service Level		
	081/2770	<1	Vehicles -	Overtop Pedestrians -	ping:	Overall Standard	- FUTURE PAGN Indicative Service Level 5	Location	
	081/2770 081/2780	<1 >100	Vehicles - -	Overtop Pedestrians - -	ping:	DEFENCE TABLE  Overall Standard:  -	PAGN Indicative Service Level 5 20	- Location	
	081/2770 081/2780 081/2790	< 1 > 100	Vehicles	Overtop Pedestrians - -	ping:	DEFENCE TABLE  Overall Standard:  -	-FUTURE -PAGN Inditative -Service Level 5 20 20	Location	

Table 4.9 Standard of Defence Table for Process Unit 5F-5

and the root of the state of the server	Defence Code	ACCURATION WAS	SDSU Fo	reshore Ass	essment		NRA Photogrammetry Analy		Comments
			Dependency	Level	Condition	Typical Profile Ref	Lower Foreshore Condition	Upper Foreshore Condition	
5F-5	081/2770	423	High	High	Stable				
	081/2770	424	High	High	Stable				
	081/2780	425	High	High	Stable				
	081/2790	426	Low	High	Stable				
	081/2790	427	Low	High	Stable				
	081/2790	428	Low	High	Stable				
	081/2800	-	<u>-</u>		_				
	081/2810		- 1	-					
	081/2820								

Table 4.10 Undermining Assessment Table for Processing Unit 5F-5

mark to a to the season of the				97	ANDARD OF DEFEN	CE TABLE , PRESE	NT		
	Tayban and the collection of t						-10		
Process Unit	Defence Code	Overflow		Overtop	ping	Overall Standard	PAGN Indicative	Location	Comments
			Vehicles	Pedestrians	Structural Damage		Service Level		
5F - 6	681/2301	> 100	-	-	-		50	Studiand	
	681/2302	> 100				-	100	N. Swanage	
	681/2303	> 100	N/A	< 1	> 10	> 10	100	N. Swanage	
	681/2304	> 100	N/A	< 1	> 100	> 100	100	Swanage	
	081/1130	> 100		-	-	*	100		
	681/2305	> 100	-	~	-		100	Swanage	
	681/2306	> 100	-	-	-	,	100	Swanage	
					STANDARD OF	DEFENCE TABLE	-FUTURE		
					STANDARD OF	DEFENCE TABLE	-FUTURE		
rocess Unit	Defence Gode	Overflow		Overtop		DEFENCE TABLE  Overall Standard		Location	Comments
rocess Unit	Defence Gode	Overslow	Vehicles	Overtopi Pedestrians					Comments
rocess Unit	Defence Gode 681/2301	Overslow > 100			ning		PAGN Indicative		Comments
			Vehicles	Pedestrians	plng Structural Damage	Overall Standard	PAGN Indicative Service Level	Location	Comments
	681/2301	> 100	Vehicles	Pedestrians -	olng Structural Damage	Overall Standard	PAGN Indicative Service Level: 50 100	Location Studiand	Comments
	681/2301 681/2302	> 100 > 100	Vehicles	Pedestrians - -	pling Structural Damage - -	Overall Standard	PAGN Indicative Service Level 3 50 100 100	Location Studiand N. Swanage	Comments
	681/2301 681/2302 681/2303	> 100 > 100 > 100	Vehicles - - - N/A	Pedestrians < 1	ping Structural Damage - - - > 5	Overall Standard  > 5	PAGN Indicative Service Level 3 50 100 100	Location Studiand N. Swanage N. Swanage	Comments

100

Swanage

Table 4.11 Standard of Defence Table for Process Unit 5F-6

> 100

681/2306

cess Unit	Defence Code	Sub Code	CPSE/SDSI	J Foreshere #	(95058ment		NRA Photogrammetry Anal	ysie.	Comments
		100	Dependency	Level	Condition	Typical Profile Ref	Lower Foreshore Condition		
5F-6	681/2301	3	High	Variable	Volatile				
	681/2302	1	High	Low	Eroding				
	681/2302	2	Medium	Low	Eroding				
	681/2303	1	High	Variable	Volatile				
	681/2303	2	Medium	Variable	Volatile				
	681/2303	3	Medium	Variable	Volatile				
	681/2303	4	Medium	Variable	Volatile				
	681/2304	1	High	Variable	Volatile				
	681/2304	2	Medium	Variable	Volatile				
	081/1130	220	High	High	Stable				
	081/1130	221	High	High	Stable				
	681/2305	1	Low	High	Stable				
	681/2305	2	High	High	Stable				
	681/2306	1	Low	High	Stable				

Table 4.12 Undermining Assessment Table for Processing Unit 5F-6

ess Unit	Defence Code	Overflow		Overtop	ping	Overall Standard	PAGN Indicative	Location	Comments
		150	Vehicles		Structural Damage		Service Level		
5F - 7	681/2307	> 100	-	-	-	-	100	Duriston Cliffs	
					Angeles de la company				
				<b>S</b> 1	fandard of Defen	CE TABLE «FUTUI	RE TO THE TOTAL PROPERTY.		
ess Unit	Defence Code	Overflow		Si	IANDARD OF DEFEN	CE:TABLE - FUTUI	RE PAGN Indicative	Location	Comments
ess Unit	Defence Code	Overflow	Vehicles	Overtop	IANDARD OF DEFEN	Overall Standard		Location	Comments
cess Unit	Defence Code	Overflow		Overtop	FANDARD OF DEFEN	Overall Standard	PAGN indicative	Location	Comments

Table 4.13 Standard of Defence Table for Process Unit 5F-7

	om il 1981 ili		I MARKET POLICE CO.	C COLO SERVICIO	(	UNDERMINING ASSESSMENT TABLE
Process Unit		Sub Code	l neces	es e la constant		NRA Prictogrammetry Analysis Companies
	Celence Code	Feet to Part One Oracle E		and the second second	45 year 800 60 4 1623 AS 8535 YES	NKA Photogrammetry Analysis Comments  Typical Profile Ref. Lower Foreshore Condition Upper Foreshore Condition
5F - 7	681/2307	1	Medium	Low	Stable	re epp., overliet Column
	681/2307	2	High	High	Stable	
				***************************************		

Table 4.14 Undermining Assessment Table for Processing Unit 5F-7

# Appendix A

Defence	qns	Ownership/	Grid Ref Start Grid Ref End Defence	Grid Ref End		Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)			Life	Built
071/1050D	_	NEWFORESTDC	SZ28769139	SZ28829137	0.07	Armour	Fr	> 5	
071/1050D	က	New Forest DC	SZ28769139	SZ28829137	0.07	Recharge	Gd		:
071/1050D	4	New Forest DC	SZ28769139	SZ28829137	70.0	Groynes	Gd	> 5	
071/1051D	_	NEWFORESTDC	SZ28829137	SZ29099128	0.28	0.28 Groynes		,	
071/1051D	2	NEWFORESTDC	SZ28829137	SZ29099128	0.28 Wall	Wall	P.O.	> 5	
071/1051D	3	3 New Forest DC	SZ28829137	SZ29099128	0.28	0.28 Recharge	Gd		
071/1051D	4	New Forest DC	SZ28829137	SZ29099128	0.28	Groynes	DG Gd	> 5	
071/1052D	1	NEWFORESTDC	SZ29099128	SZ29279120	0.18	Groynes	1	> 5	
071/1052D	2	2 NEWFORESTDC	SZ29099128	SZ29279120	0.18	Apron	<u>L</u>	> 5	
071/1052D	3	NEWFORESTDC	SZ29099128	SZ29279120	0.18 Wall	Wall	P. P	> 5	
071/1052D	4	4 New Forest DC	SZ29099128	SZ29279120	0.18	0.18 Recharge	P. O		
071/1052D	5	5 New Forest DC	SZ29099128	SZ29279120	0.18	0.18 Groynes	<del>Q</del> q	> 5	
071/1053D	*	1 NEWFORESTDC	SZ29279120	SZ29489114	0.23	0.23 Bastion	ĭ	> 5	
071/1053D	2	2 NEWFORESTDC	SZ29279120	SZ29489114	0.23	Groynes	29	> 5	
071/1053D	3	3 NEWFORESTD.C.	SZ29279120	SZ29489114	0.23	Apron	L	> 5	
071/1053D	4	NEWFORESTD.C.	SZ29279120	SZ29489114	0.23 WRtn	WRtn	Gd	> 5	
071/1053D	5	New Forest DC	SZ29279120	SZ29489114	0.23	0.23 Recharge	P5		
071/1053D	9		SZ29279120	SZ29489114	0.23	0.23 Groynes	Gd	> 5	
071/1054D	~	1 NEWFORESTD.C.	SZ29489114	SZ29959090	0.63	Pitching	Gd	> 55	1991
071/1054D	2	2 NEWFORESTD.C.	SZ29489114	SZ29959090	0.63	Embkmt	РЭ	> 5	1991
071/1055D	~	NEWFORESTD.C.	SZ29959090	SZ31028984	1.54	Embkmt	Gd	> 5	1991
081/1010	200	200 CHRISTCHURCH	SZ17979098	SZ18299152	0.89	Banks	ģ	> 5	
081/1020	201		SZ18289158	SZ18339198	08.0	Banks	<u>-</u>	> 5	1960
081/1030	202	CHRISTCHURCH	SZ17299238	SZ16559184	3.30	3.30 Banks	<b>₽</b>		
081/1040	203	203 POOLEBC	SY99359008	SY99939012	0.80 Wall	Nall	Gd	\ \ \ \ \	
081/1040	204	204 POOLEBC	SY99359008	SY99819002	0.69	0.69 Groynes	Gd	V 55	
081/1040	205	205 POOLEBC	SY99939012	SZ00139013	0.10	Banks	Pr	> 22	
081/1050	206		***********	SZ00319288	1.40	Embkmt	<del>Gd</del>	۸ ۲	
081/1060	207	ite) o		SZ01699022	0.30	Embkmt	<del>O</del> d	٧ ج	1990
081/1060	208	208 POOLEBC	SZ01379021	SZ01589017	0.20	Bkwtrs	Qq	> 5	

Table A.1: Coastal Defences

Defence	gns	Ownership/	<b>Grid Ref Start</b>	Grid Ref Start Grid Ref End	Defence	Structure Type   Condition	Condition	Recidinal	Vaar
Code	Code	Responsibility	Coords	Coords	Length			Life	Built
			***************************************		(km)		novement and the second		
081/1060	209	POOLEBC	SZ01399025	SZ01699022	0.30	Revet	Gd	۷ ت	1990
081/1060	210		SZ01699022	SZ01869018	0.30		99	> 2 > 5	2
081/1060	211		SZ01869018	SZ02109012	0.16	Banks	Gd	> 55	:
081/1060	212	POOLEBC	SZ02109018	SZ02479064	09.0	Pitching	L	۸ ک	
081/1060	443	EA	SZ01509030	SZ01709030	0.20	Wall	ŭ	2 to 5	
081/1070	213	213 POOLEBC	SZ02479064	SZ03059066	09:0	0.60 Pitching	Ţ	> 5	
081/10/0	214	POOL EBC	SZ03059066	SZ03189048	0.20	Wall	Ā	> 5	
081/1080	215	POOLEBC	SZ04088929	SZ04288905	0.30	Gabions	Bd	< 2	
081/1090	216	216 POOLE BC	SZ02049066	SZ02099087	0.20	Wall	gg	> 5	
081/1110	217	POOLE BC	SZ02539094	SZ02629076	0:30	Wall	I	> 5	
081/1120	218	218 PBC&HARBOUR COMMISSIONERS	SZ04298905	SZ04908854	1.00 Wal	Wall	Pg	> 5	
081/1120	219	UR COMMISSIONER	SZ04908854	SZ04308769	1.20	SpWI	PO	> 5	
081/1130	220	220 PURBECKDC	SZ03107950	SZ03507870	1.20	1.20 Groynes	Bq	2 to 5	
081/1130	221	221 PURBECKDC	SZ03107950	SZ03507870	1.20 Wal	Wall	L	> 5	1938
081/1140	222	222 PURBECKDC		SZ03158772	1.25	1.25 Armour	වි	> 5	1989
081/2010	320	320 PRIVATE VARIOUS		SZ17289230	0.10	Banks	۵	> 5	
081/2010	321	321 PRIVATE VARIOUS		SZ17289230	0.10 Wal	Wall	Pŗ	V 55	
081/2020	322	322 PRIVATE VARIOUS	SZ17289230	SZ17359226	0.07 Wall	Wall	L	> 5	
081/2030	323	323 PRIVATE VARIOUS		SZ17929192	0.75 Wal	Wall	Pŗ	2 to 5	
081/2040	324	324 PRIVATE VARIOUS		SZ17979199	0.30	Embkmt	Ā	2 to 5	:
081/2050	325	325 PRIVATE VARIOUS		SZ18059207	0.20	Wall	Pr	2 to 5	
081/2060	326			SZ18199203	0.14	Wall	i i	> 5	:
081/2060	327	327 AVONMOUTHHOTEL (THF)		SZ18199203	0.14	Embkmt	L	v 5	
081/2070	328	328 PRIVATE VARIOUS	SZ18229203	SZ18249202	0.07	Wall	Ł	V 55	
081/2080	329	329 PRIVATE VARIOUS		SZ18329200	0.02	Wall	<u>L</u>	V 55	
081/2090	330	330 PRIVATE	_	SZ03178760	0.05	Wall	P	2 to 5	
081/2100	331	PRIVATE	SZ03168769	SZ03168770	0.05	Wall	, L	ဲ့ပ	
081/2110	332	PRIVATE	SZ03158763	SZ03168769	0.10 Wal	Vall	Į.	v 5	ì
081/2120	333	PRIVATE	-	SZ03158763	0.02 Wall		Gd	× 5	
081/2130	334	PRIVATE	SZ03068760	SZ03138762	0.05 E	(S		V 35	
							-		

Defence	gns	Ownership/	Grid Ref Start Grid Ref End Defence	Grid Ref End		Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)			Life	Buit
081/2130	335	PRIVATE	SZ03068760	SZ03138762	0.05	Wall		> 5	
081/2140	336	PRIVATE	SZ02908745	SZ02958750	0.10	Groynes	L	1	!
081/2140	337	PRIVATE	SZ02958750	SZ03058759	0.14	Groynes	<u>L</u>	> 5	
081/2140	338	PRIVATE	SZ02758740	SZ03068760	0.37	Wall	4	> 5	
081/2150	339	339 PRIVATE VARIOUS	SZ03848764	SZ03608748	0.30 Wall	Wall	Ā	> 5	
081/2160	340	340 POOLEHARBOUR COMMISSIONERS	SZ04278908	SZ04788878	0.61	SpWI	Ŧ	> 5	1895
081/2170	341	POOLEHARBOUR COMMISSIONERS	SZ04788878	SZ04918854	0.28	Banks	Gd	> 5	
081/2170	342	POOLEHARBOUR COMMISSIONERS	SZ04788878	SZ04918854	0.28	SpWI	L.	> 5	1895
081/2180	343	POOLEHARBOUR COMMISSIONERS	SZ04918854	SZ04908827	0.25	Banks	Ŀ	> 5	
081/2180	344	POOLEHARBOUR COMMISSIONERS	SZ04918854	SZ04908827	0.25	Wall	Pr	> 5	
081/2190	345	POOLEHARBOUR COMMISSIONERS	SZ04908827	SZ04328768	0.89 Wall	Wall	L	က ^	:
081/2200	346	346 PRIVATE VARIOUS	SZ03808970	SZ03858966	0.10	Banks	Ā	> 5	
081/2210	347	347 PRIVATE VARIOUS	SZ03858966	SZ04088929	0.44 Wall	Wall	Ţ	> 5	
081/2220	348	348 SALTERNSMARINA	SZ03708975	SZ03658972	0.12	Pitching	Bd		
081/2220	349	349 SALTERNSMARINA	SZ03708975	SZ03658972	0.12	Banks	Pŗ	V 55	
081/2230	350	350 SALTERNSMARINA	SZ03658972	SZ03628963	0.09	Banks	Gd	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
081/2230	351	351 SALTERNSMARINA	SZ03658972	SZ03628963	0.09 Wall	Wall	<u>G</u> d	> 5	
081/2240	352	SALTERNSMARINA	SZ03628963	SZ03508943	0.23	Armour	L	> 5	
081/2240	353	SALTERNSMARINA	SZ03628963	SZ03508943	0.23	SpWI	Gd	> 5	
081/2250	354	354 SALTERNSMARINA	SZ03428942	SZ03428942	0.01	Bkwtrs	<sub>Gd</sub>	> 5	
081/2250	355	SALTERNSMARINA	SZ03508943	SZ03468940	70.0	Wall	P9	> 5	
081/2260	356	SALTERNSMARINA	SZ03468940	SZ03738968	0.41	Wall	<del>g</del> q	× 5	
081/2270	357	SALTERNSMARINA	SZ03738968	SZ03768972	0.11	Wall	L.	> 5	
081/2270	358	SALTERNSMARINA	SZ03738968	SZ03768972	0.11	Wall	ලිය	× 5	
081/2280	359	SALTERNSMARINA	SZ03768972	SZ03748967	60.0	Wall	Ţ.	i	:
081/2290	360	SALTERNSMARINA	SZ03748967	SZ03748966	0.02	Wall	වි		
081/2300	361	SALTERNSMARINA	SZ03748965	SZ03748965	0.01	Bkwtrs	P.O	v V	
081/2300	362	362 SALTERNSMARINA	SZ03748966	SZ03748965	0.02	Pitching	Pr	2 to 5	
081/2300	363	SALTERNSMARINA	SZ03748966	SZ03748965	0.02	Banks	Ŀ	က	
081/2310	364	364 SALTERNSMARINA	SZ03748965	SZ03808970	0.05	Wall	7	2 to 5	

Defence	gng	Ownership/	<b>Grid Ref Start</b>	Grid Ref Start Grid Ref End Defence	Defence	Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)	;		Life	Built
081/2320	365	365 LILLIPUTS.C.	SZ03579024	SZ03659020	0.07	Wall	P	2 to 5	
081/2330	366	PARKWAYMARINE	SZ03659020	SZ03679018	0.05 Wa	Wall	à		;
081/2340	367	POOLEHARBOUR COMMISSIONE	SZ00629035	SZ00659034	0.02 Wa	Wall	à	2 to 5	
081/2350	368	368 POOLEHARBOUR COMMISSIONERS	SZ00659034	SZ00709031	0.07 Wal	Wall	L	5	
081/2360	369	POOLEHARBOUR COMMISSIONE	SZ00709031	SZ00809028	0.10 Wal	Wall	ŭ	> 5	
081/2370	370	POOLEHARBOUR COMMISSIONE	SZ00809028	SZ00849026	0.05	Wall	L	v 55	
081/2380	371	POOLEHARBOUR COMMISSIONERS	SZ00849026	SZ01059024	0.20	Wall	ŭ	> 5	
081/2390	372	POOLEHARBOUR COMMISSIONERS	SZ01059024	SZ01219023	0.17	Wall	1	> 5	!
081/2400	373	373 POOLEHARBOUR COMMISSIONERS	SZ01219023	SZ01399022	0.15 Wall	Wall	L	V 55	
081/2410	374	POOLEHARBOUR COMMISSIONERS	SZ01399020	SZ01419017	0.03	Bkwtrs	<u>a</u>	> 5	
081/2410	375	POOLEHARBOUR COMMISSIONERS	SZ01399022	SZ01419025	0.03	Wall	ī	> 5	
081/2411	-	EA	SZ01359026	SZ01659025	0.25	Embkmt	L	2 to 5	
081/2420	376	376 POOLEHARBOUR COMMISSIONERS	SZ01419017	SZ01509015	0.07	Bkwtrs	ă.	> 5	
081/2420	3//	377 POOLEHARBOUR COMMISSIONERS	SZ01419025	SZ01509024	0.07	Wall	P	> 5	
081/2430	378	POOLEHARBOUR COMMISSIONERS	SZ01509015	SZ01589017	0.10	Bkwtrs	4	> 5	
081/2430	379	POOLEHARBOUR COMMISSIONERS	SZ01509024	SZ01589028	0.10	0.10 Banks	Qq	> 5	
081/2450	381	PRIVATE	SZ01209105	SZ00849103	0.38	Pitching	1	> 5	
081/2450	382	PRIVATE	SZ01209105	SZ00849103	0.38	0.38 Banks	正	v 5	
081/2460	383	383 PRIVATE	SZ00849103	SZ00859091	0.14 Wal	Nall	<del>Q</del> q	> 5	
081/2470	384	384 PRIVATE	SZ00859091	SZ00789078	0.20 Wal	Nall	Bd	2 to 5	:
081/2480	385	385 PRIVATE		SZ00679063	0.17	Wall	L	> 5	
081/2490	386		~	SZ00659061	0.05	Wall	<u>P</u>	< 2	:
081/2500	387	**************************************		SZ00599050	0.12	Wall	<u></u>	> 5	
081/2510	388		SZ00599050	SZ00599049	0.01	Wall	Pr	2 to 5	
081/2520	389			SZ00589042	0.13	Wall	L L	\ \ \ \	
081/2530	330		SZ00589042	SZ00629036	0.07	Wall	Bd	2 to 5	:
081/2540	391		SZ00479045	SZ00549070	0.28	Wall	Ŀ		
081/2550	392	SS C		SZ00569029	0.07	Wall	1	\ \ \	:
081/2560		O		SZ00649024	0.07	Wall	Ŀ	:	:
081/2570	394	POOLEHARBOUR COMMISSIONERS C	SZ00799022	SZ00709023	0.07	Wall	Ţ.	> 5	

Code 081/2580 081/2590 081/2590	Code								3
081/2580 081/2590 081/2590		Responsibility	Coords	Coords	Length (km)			<u>.</u>	Built
081/2590 081/2590	395	395 PRIVATE	SZ00809018	SZ00799022	0.05	Wall	1	> 5	
081/2590	396		SZ00819017	SZ00809018	0.01	Apron	·L	> 5	
	397	POOLEHARBOUR COMMISSIONERS C	SZ00819017	SZ00809018	0.05	Wall	L	> 5	:
081/2600	398	POOLEHARBOUR COMMISSIONERS C	SZ00849020	SZ00819017	0.05	Wall	à.	> 5	
081/2610	399	POOLEHARBOUR COMMISSIONERS C		SZ00849020	0.02 Wal	Wall		\ \ \ \	
081/2620	400	400 PHC/LESSEE	SZ00859018	SZ00849018	0.02	Wall	Ā	2 to 5	
081/2630	401	401 PHC/LESSEE	SZ00869020	SZ00859018	0.02	Wall		> 5	
081/2640	402	PHC/LESSEE	SZ00169015	SZ00139007	0.07	Armour	Gd	> 5	
081/2640	403		SZ00169015	SZ00139007	70.0	Banks	95	> 5	1
081/2650	404	PHC/LESSEE	SZ00139007	SZ00149007	0.01	Bkwtrs	Gd	> 5	
081/2650	405	PHC/LESSEE	SZ00139007	SZ00299003	0.17	Wall	25	> 5	
081/2660	406	PHC/LESSEE	SZ00299003	SZ00298986	0.17	Pitching	<u>G</u> d	> 5	
081/2660	407	PHC/LESSEE	SZ00299003	SZ00298986	0.17	Banks	<u>G</u> d	> 5	; !
081/2670	408	PHC/LESSEE	SZ00298986	SZ00558976	0.62	Banks	P9	> 22	
081/2670	409	409 PHC/LESSEE	SZ00298986	SZ00558976	0.62	Armour	gq	> 5	
081/2680	410	410 POOLEHARBOUR COMMISSIONERS	SZ00558976	SZ00888976	0.38 Wall	Wall	Gd	> 5	1988
081/2690	411	411 POOLEHARBOUR COMMISSIONERS	SZ00888976	SZ00948993	0.25	0.25 Armour	Ī	> 5	:
081/2690	412	412 POOLEHARBOUR COMMISSIONERS	SZ00888976	SZ00948993	0.25	Banks	L	> 5	
081/2700	413	413 POOLEHARBOUR COMMISSIONERS	SZ01058993	SZ01068993	0.01	Bkwtrs	Bd	2 to 5	
081/2700	414	414 POOLEHARBOUR COMMISSIONERS	SZ00948993	SZ01068993	0.12	Armour	Gd	<u> </u>	
081/2700	415	POOLEHARBOUR COMMISSIONERS	SZ00948993	SZ01068993	0.12	Banks	P9	7 5	
081/2710	416	416 POOLEHARBOUR COMMISSIONERS	SZ01068993	SZ01059009	0.16	Wall	1	۷ ک	:
081/2720	417	417 POOLEHARBOUR COMMISSIONERS	SZ01059009	SZ01009017	60.0	Wall	Pr	۷ ئ	
081/2730	418		SZ01009017	SZ00939019		Brwork	Pr	V 53	:
081/2730	419	POOLEHARBOUR COMMISSIONE	SZ01009017	SZ00939019	0.07	Wall	L	V LC	
081/2740	420	420 POOLEHARBOUR COMMISSIONERS	SZ00939019	SZ00869020	0.07	Wall	<u>L</u>	> 5	
081/2750	421	PRIVATE (VARIOUS)	SY98939018	SY99359010	0.47	Wall	Ţ	> 2	
081/2760	422	PRIVATE (VARIOUS)	SY98889022	SY98939018	0.05	Wall	වී	> 21	1990
081/2770	423	Well-state and make a second s	SZ03628297	SZ03648668	4.30	Embkmt	L	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	:
081/2770	424	424 NATIONAL TRUST	SZ03528316	SZ03468333	0.16	0.16 Gabions	Bd	< 2	

Table A.1: Coastal Defences

Defence	Sub	Ownership/	Grid Ref Start Grid Ref End		Defence	Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)	:		Life	Built
081/2780	425	425 NATIONALTRUST	SZ03698292	SZ03628297	0.07	Wall	ă	2 to 5	
081/2790	426	426 NATIONALTRUST	SZ03758285	SZ03758289		Armour			:
081/2790	427	427 NATIONALTRUST	SZ03758285	SZ03698292	0.07	Gabions	à	< 2	:
081/2790	428	NATIONALTRUST	SZ03758285	SZ03698292		Banks	Ţ	< 2	!
081/2800	429		SZ04018256	SZ03858285	0.30	Banks	L	> 5	:
081/2810	430	PRIVATE	SZ04088250	SZ04018256	0.10	Gabions	<u>L</u>	> 5	:
081/2820	431			SZ04088250	0.26	Banks	Pŗ	> 5	
571/2757	-		SZ31868974	SZ31818971	0.06	Breastwork	Class 2	> 10	1980
571/2757	2			SZ31788971	0.04 Wal	Wall	Class 4	5 - 10	1850
571/2757	3			SZ31578970	0.15	0.15 Breastwork	Class 3	5 - 10	1970
571/2757	4		_	SZ31508971	0.03	Breastwork	Class 3	5 - 10	1970
571/2757	5	ENGLISH HERITAGE		SZ31468972	0.04	0.04 Breastwork	Class 2	> 10	1980
571/2757	ဖ		SZ31818971	SZ31578970	0.25	Armour	Class 3	> 10	1980
571/2757	7	ENGLISH HERITAGE	SZ31868974	SZ31468972	0.41	Groynes	Class 3	> 10	1970
571/2758	-	NEW FOREST DC / HAMPSHIRE CC	SZ31468972	SZ29929079	1.87	Beach Ridge			
571/2758	2	NEW FOREST DC		SZ29929079	1.87	Recharge	Class 1	5 - 10	1996
571/2759	***		SZ29929079	SZ29489113	0.54	Embankment	Class 2	> 10	
571/2759	2	NEW FOREST	SZ29929079	SZ29489113	0.55	Revetment	Class 1	> 10	1996
571/2760	_	1 NEW FOREST DC		SZ29279121	0.23 Wal	Vall	Class 2	> 10	1964
571/2760	2	2 NEW FOREST DC		SZ29279121	0.23	Apron	Class 3	> 10	1964
571/2760	8	3 NEW FOREST DC		SZ29259122	0.25 (	Groynes	Class 2	> 10	1964
571/2761	-	. 1.		SZ29109129	0.18 \	Wall	Class 3	> 10	1960
571/2761	2	2 NEW FOREST DC		SZ29109129	0.18 /	Apron	Class 3	> 10	1960
571/2761	က			SZ29109129	0.16	Groynes	Class 2	> 10	1960
571/2762	-	1 NEW FOREST DC	SZ29109129	SZ28849138	0.28 Wal		Class 3	> 10	1960
571/2762	7	2 NEW FOREST DC	SZ29099128	SZ28849138	0.28	Wall	Class 3		1964
571/2762	3	3 NEW FOREST DC	SZ29099128	SZ28849138	0.28	Groynes	Class 2	5 - 10	1960
571/2763	~	1 NEW FOREST DC	SZ28849138 S	SZ28769139	0.08	Wall	Class 2	> 10	1980
571/2763	2	<ul> <li>I</li> </ul>	SZ28849138 S	SZ28769139	0.08	Groynes	2	5-10	1970
571/2763	3	3 NEW FOREST DC	SZ28849138 S	SZ28769139	0.08	:	က	> 10	1991

Defence	gng	Ownership/	Grid Ref Start Grid Ref End	Grid Ref End	Defence	Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)			<u> </u>	Built
571/2764		NEW FOREST DC	SZ28769139	SZ28609146	0.17	Wall	Class 3	> 10	1960
571/2764	2	NEW FOREST DC		SZ28609146	0.17	Groynes	Class 2	5 - 10	1960
571/2765		NEW FOREST DC	SZ28609146	SZ27739178	0.92	Cliff / Scarp			
571/2765	2	2 NEW FOREST DC	SZ28609146	SZ27859170	0.78	Wall	Class 2	> 10	1970
571/2765	က	3 NEW FOREST DC		SZ27859170	0.78	Toe Piling	Class 2	> 10	1970
571/2765	4	4 NEW FOREST DC	SZ28609146	SZ27859170	0.78	Groynes	Class 3	5 - 10	1970
571/2765	.S	5 NEW FOREST DC	SZ28149160	SZ27949167	0.21	Armour	Class 2	> 10	1970
571/2765	ဖ	6 NEW FOREST DC	SZ28379153	SZ28199158	0.18	Revetment	Class 1	> 10	1995
571/2765	7	7 NEW FOREST DC	SZ28199158	SZ28089161	0.12	Revetment	Class 1	> 10	1996
571/2766	<b>~</b>	1 NEW FOREST DC	SZ27739178	SZ25359253	2.51	Cliff / Scarp			
571/2767	<b>~~</b>	1 NEW FOREST DC	SZ25359253	SZ24939265	0.43	Cliff / Scarp			:
571/2767	2	SOUTHERN WATER	SZ25359253	SZ25309254	0.03	Armour	Class 3	> 10	1980
571/2768	<b>V</b>	NEW FOREST DC	SZ24939265	SZ23089298	1.88	Cliff / Scarp			
571/2768	2	2 NEW FOREST DC	SZ24939265	SZ23089298	1.88	Revetment	Class 1	> 10	1990
571/2768	3		SZ24939265	SZ23089298	1.88	Groynes	Class 1	> 10	1977
571/2769	7	NEW FOREST DC		SZ21799313	1.30	Cliff / Scarp			
681/2301	_	SHELL BAY BOATYARD & CAFE	SZ03488648	SZ03518650	0.03	Revetment	Class 2	5 - 10	1980
681/2301	2	SHELL BAY BOATYARD &	SZ03518650	SZ03558651	0.03	Revetment	Class 2	> 10	1980
681/2301	က	SHELL BAY BOATYARD & CAFE	SZ03518648	SZ03558651	0.05	Wall	Class 2	× 10	1980
681/2302	_	PURBECK DC		SZ03368024	0.24	Groynes	Class 4	× 5	1962
681/2302	2	2 PURBECK DC	SZ03468042	SZ03368024	0.24	Cliff / Scarp			
681/2303	****	PURBECK DC		SZ03107965	09.0	Wall	Class 4	5 - 10	1962
681/2303	2	PURBECK DC		SZ03107965		Groynes	Class 4	5 - 10	1962
681/2303	က	PURBECK DC	SZ03368024	SZ03107965	09.0	Wall	Class 3	~	1962
681/2303	4	PURBECK DC		SZ03107965	0.60	Toe Piling	Class 3		1962
681/2304		1 PURBECK DC / DORSET CC	SZ03107965	SZ03087914	50	Wall	Class 2		1930
681/2304	2	2 PURBECK DC	SZ03107965	SZ03087914	0.50	Groynes	Class 4	5-10	1930
681/2305		1 WESSEX WATER		SZ03787865	0.17	Wall	Class 3	. v	1950
681/2305	2	PRIVATE		SZ03787865	0.17 Wa		Class 3	< 5 م	1980
681/2306		WESSEX WATER	SZ03787865	SZ03987865	0.20	20 Wall	Class 3	5 - 10	1950

Table A.1: Coastal Defences

Defence	gns	Ownership/	Grid Ref Start	Grid Ref Start Grid Ref End Defence		Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)	•		Life	Built
681/2307	_	PURBECK DC	SZ03557818	SZ03517812		Revetment	Class 1	> 10	1989
681/2307	7	2 PURBECK DC	SZ03557818	SZ03517812	0.06	Gabions	Class 2	> 10	1989
681/2401	-	POOLE BC	SZ07138993	SZ06028931		Vall	Class 3	> 10	1960
681/2401	2	POOLE BC	SZ06028931	SZ05928920	0.15 Wal	/all	Class 2	> 10	1985
681/2401	က		SZ06028931	SZ05928920	0.15 S	Splash Wall	Class 2	> 10	1985
681/2401	4		SZ07138993	SZ05928920	1.44 G	Groynes	Class 4	< 5	1980
681/2402	~	POOLE BC	SZ05928920	SZ05818911	0.13 M	Wall	Class 2	> 10	1970
681/2402	2	2 POOLE BC	SZ05928920	SZ05818911	0.13 G	Groynes	Class 4	> 10	1980
681/2403	•	POOLE BC	SZ05818911	SZ05488882	0.44 R	Recurved Wall	Class 2	> 10	1970
681/2403	2	2 POOLE BC	SZ05818911	SZ05488882	0.44 G	Groynes	Class 4	< 5	1980
681/2404	-	1 POOLE BC	SZ05488882	SZ05378867	0.44 R	d Wall	Class 3	> 10	1970
681/2404	2	2 POOLE BC	SZ05488882	SZ05378867	0.44		Class 4	> 10	1970
681/2404	3	3 POOLE BC	SZ05488882	SZ05378882	0.44	Vall	Class 2	> 10	1970
681/2405	-	1 POOLE BC	SZ05378867	SZ05058834	0.45 W		Class 2	> 10	1960
681/2405	2	U	SZ05378867	SZ05058834	0.45 G	Groynes	Class 2	> 10	1980
681/2406	-	0.000	SZ05058834	SZ04648787	0.63 R	int	Class 3	5 - 10	1960
681/2407	-	7 St. Markatan and A. S. Carlottan and A. S. C	SZ04648787	SZ04588779	0.10 R		Class 2	> 10	1970
681/2407	2	7.70	SZ04588779	SZ04468762	0.20 Wall		Class 2	> 10	1960
681/2407	က	Q	SZ04468762	SZ04358752	0.16 R	Recurved Wall	Class 2	> 10	1960
681/2408	-		SZ04358752	SZ04268740	0.15 Br	Breastwork	Class 2	> 10	1970
681/2408	2	7,000,000,000,000,000,000,000,000,000,0	SZ04358752	SZ04268740	0.15 R	-	Class 1	> 10	1996
681/2408	က	POOLE BC	SZ04358752	SZ04268740	0.15 G	Groynes	Class 1	> 10	1996
681/2409	2		SZ04268740	SZ04208731	0.10 R	ant l	Class 1	> 10	1996
681/2409	က	Q	SZ04268740	SZ04208731	0.10 G	Groynes	Class 1	> 10	1996
681/2410	-		SZ04208731	SZ04118721	3		Class 1	> 10	1990
681/2410	က	The state of the s	SZ04208731	SZ04118721		Revetment	Class 1	> 10	1996
681/2410	4		SZ04208731	SZ04118721	0.15 G	:	Class 1	> 10	1996
681/2411	-	POOLE BC	SZ04118721	SZ04078718	0.10 Wall		Class 1	> 10	1990
681/2411	ਲ		SZ04118721	SZ04078718	0.10 Re	Revetment (	Class 1	× 10	1996
681/2411	4	4 POOLE BC	SZ04118721	SZ04078718	0.10 Groynes	:	Class 1	× 10	1996

Defence	gns	Ownership/	Grid Ref Start Grid Ref End		Defence	Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)			Life	Built
681/2412		PRIVATE	SZ04078718	SZ04038715	0.05	Wall	Class 2	> 10	1970
681/2412	2		SZ04038715	SZ03978712	0.07	Piling	Class 4	^ 5	1960
681/2412	က	PRIVATE	SZ04038715	SZ03978712	0.07	Wall	Class 3	> 10	1960
681/2412	4	4 PRIVATE	SZ03978712	SZ03908707	0.08 Wal	Wall	Class 3	> 10	1970
681/2412	2	5 PRIVATE	SZ03978712	SZ03938710	0.04	Toe Piling	Class 2	> 10	1980
681/2412	9	6 PRIVATE	SZ03978712	SZ03938710	0.04	Wall	Class 2	> 10	1980
681/2412	7	7 POOLE BC		SZ03908707	0.20	Recharge	Class 2	5 - 10	1992
681/2412	8			SZ03908707	0.08	Armour	Class 2	> 10	1970
681/2412	6			SZ03908707	0.20	Revetment	Class 1	> 10	1996
681/2412	10			SZ03908707	0.20	Groynes	Class 1	> 10	1996
681/2413	-	PRIVATE		SZ03768702	0.21	Recurved Wall	Class 1	> 10	1990
681/2413	2	PRIVATE		SZ03768702	0.21	Toe Piling	Class 1	> 10	1990
681/2413	က	PRIVATE	SZ03908707	SZ03768702	0.21	Revetment	Class 1	> 10	1990
681/2413	4	PRIVATE	SZ03908707	SZ03768702	0.21	Groynes	Class 1	> 10	1990
681/2414	*	POOLE BC	SZ03768702	SZ03738704	0.04	Wall	Class 3	> 10	1960
681/2414	2		SZ03768702	SZ03738704	0.04	Toe Piling	Class 2	> 10	1960
681/2415	•	PRIVATE		SZ04308769	1.42	Wall	Class 4	< 5	1960
681/2416		POOLE BC		SZ04908830	06.0	Wall	Class 2	5 - 10	1982
681/2417	<b>4</b>	POOLE BC	SZ04908830	SZ04258910	1.25	Wall	Class 2	< 5	1950
681/2417	2	2 POOLE BC	SZ04288904	SZ04278906	0.15	Groynes	Class 3	5 - 10	1950
681/2418	_	Ų	SZ04258910	SZ04038933	0.32	Gabions	Class 4	۸ گ	1975
681/2419	-			SZ03788967	0.45	Wall	Class 3	v کا	1960
681/2420	_		SZ03518936	SZ03568968	0.39	Breakwater	Class 1	> 10	1986
681/2420	2	PRIVATE		SZ03578963	0.10	Revetment	Class 1	> 10	1986
681/2421	~~	O	SZ03568968	SZ03338989	0.28	Wall	Class 4	\ ا	1930
681/2422	_	PRIVATE	SZ03338989	SZ03109038	0.88	Wall	Class 2	> 10	1960
681/2422	2	PRIVATE	SZ03049014	SZ02899027		Breakwater	Class 1	> 10	1996
681/2423	-	. The second sec	SZ03219044	SZ03069066		Revetment	Class 3	> 10	1970
681/2423	2	POOLE BC	SZ03219044	SZ03169066	0.27	Wall	Class 2	> 10	1970
681/2424	_	1 POOLE BC	SZ03069066	SZ02109016	1.21	Revetment	Class 4	< 5	1970

Defence	Sub	Ownership/	<b>Grid Ref Start</b>	Grid Ref Start Grid Ref End	Defence Structure	Structure Type Condition	ndition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)			Life	Built
681/2425	~	POOLE BC	SZ01869018	SZ01719023	0.16 Revetment	nt Class	SS 1	> 10	1980
681/2426	~	NRA	SZ01719023	SZ01589025	0.13 Revetment	<u>:</u>	ss 2	> 10	1980
681/2427	•	POOLE HC	SZ01589017	SZ01369020	0.26 Breakwater		ss 4	< 5	1920
681/2428	-	PRIVATE	SZ01509026	SZ01369023	0.15 Wall	Class	SS 1	> 10	1990
681/2429	_	1 POOLE HC	SZ01369023	SZ00809027	0.57 Wall	Class	ss 2	> 10	1960
681/2429	2	POOLE HC	SZ01239023	SZ01059025	0.19 Piling	Class	ss 1	> 10	1980
681/2430	7	POOLE HC	SZ00809027	SZ00659035	0.19 Wall	Class	SS 3	5 - 10	1950
681/2431	_		SZ00659035	SZ00849095	0.75 Piling	Class	S 3	5 - 10	1970
681/2432	-	PRIVATE	SZ00849095	SZ01209106	0.45 Revetment	nt Class	2	> 10	1980
681/2433	-	POOLE BC	SZ01209106	SZ01229110	0.05 Wall	Class 2	2	> 10	1970
681/2434	_	POOLE BC	SZ01229110	SZ00509280	2.10 Revetment		_	> 10	1986
681/2435	-	1 BR	SZ00659222	SY99329211	1.35 Revetment	nt Class 2		> 10	1970
681/2435	2	2 BR	SZ00659222	SY99329211	1.35 Embankment	ent Class 2		> 10	1900
681/2436	-	PRIVATE	SZ00559070	SZ00599029	0.50 Wall	Class	2	> 10	1960
681/2437	~	POOLE HC	SZ00599029	SZ01009017	0.50 Piling	Class 3		5 - 10	1944
681/2437	2	POOLE HC	SZ01009017	SZ01078993	0.26 Piling	Class	2	> 10	1929
681/2437	က	3 POOLE HC	SZ01078993	SZ00938977	0.32 Piling	Class	2	> 10	1972
681/2437	4	4 POOLE HC	SZ00938977	SZ00748973	0.23 Piling	Class 2	~	> 10	1984
681/2437	2	5 POOLE HC	SZ00748973	SZ00568974	0.20 Piling	Class		> 10	1988
681/2438	~	1 POOLE HC	SZ00568974	SZ00129006	0.41 Breakwate		2	> 10	1983
681/2438	2	2 POOLE HC	SZ00129006	SZ00139013	0.16 Revetment	rt Class	2	> 10	1983
681/2439	_	PRIVATE	SZ00139013	SY99939011	0.21 Beach Ridge	ge			;
681/2440	_		SY99939011	SY99359008	0.61 Wall	Class	4	< 5	1960
681/2440	7	U	SY99939011	SY99359008	0.61 Groynes	Class	2	> 10	1970
681/2441	-	1 PRIVATE	SY99359008	SY98419044	1.03 Wall	Class	2	> 10	1970
681/2442	•		SY98379044	SY98319047	0.09 Gabions	Class	0	< 5	1980
681/2443	-	7. 200 100 100 100 100 100 100 100 100 100	SY97669074	SY97539081	0.15 Gabions	Class 4			1980
681/2443	2		SY97539081	SY97319098	0.28 Gabions	Class		< 5	1980
681/2444	-	PRIVATE (	SZ03788967	SZ03528938	0.41 Breakwate		:	. 10	1986
681/2501	F		SZ16959096	SZ17109092	0.16 Gabions	Class			1987

Defence	gng		Grid Ref Start Grid Ref End	Grid Ref End	Defence	Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)			Life	Built
681/2502	-	1 CHRISTCHURCH BC	SZ18149096	SZ18219102	0.08	Armour	Class 1	> 10	1990
681/2502	2	2 CHRISTCHURCH BC	SZ18149096	SZ18259135	0.38	Bank		5 - 10	1900
681/2503	_	1 CHRISTCHURCH BC	SZ18379135	SZ18329114	0.22	Revetment	Class 2	5 - 10	1980
681/2503	2	2 CHRISTCHURCH BC	SZ18379135	SZ18329114	0.22	Groynes	Class 2	> 10	1980
681/2504	_	CHRISTCHURCH BC	SZ18329114	SZ18189091	0.27	Wall	Class 2	> 10	1960
681/2504	7	2 CHRISTCHURCH BC	SZ18329114	SZ18189091	0.27	Splash Wall	Class 2	> 10	1960
681/2504	က	3 CHRISTCHURCH BC	SZ18329114	SZ18189091	0.27	Toe Piling	Class 2	> 10	1960
681/2504	4		SZ18329114	SZ18189091	0.27	Recharge	Class 2	> 10	1990
681/2504	5		SZ18329114	SZ18189091	0.27	Groynes	Class 1	> 10	1990
681/2505	<b>~~~</b>	CHRISTCHURCH BC	SZ18189091	SZ18069060	0.34	Revetment	Class 3	\ م	1965
681/2505	2		SZ18189091	SZ18069060	0.34	Groynes	Class 3	< 5	1965
681/2505	က	CHRISTCHURCH BC	SZ18189091	SZ18189091	90.0	Armour	Class 1	> 10	1990
681/2506	~	BOURNEMOUTH BC	SZ18069060	SZ17829039	0.36	Revetment	Class 1	> 10	1987
681/2506	2	BOURNEMOUTH BC	SZ18069060	SZ17829039	0.36	Groynes	Class 1	> 10	1987
681/2506	3	BOURNEMOUTH BC	SZ18069060	SZ17829039	0.36	Groynes	Class 1	> 10	1965
681/2506	4	BOURNEMOUTH BC	SZ18069060	SZ18069060	0.04	Armour	Class 2	> 10	1991
681/2506	5	BOURNEMOUTH BC	SZ18079059	SZ18079059	0.02	Groynes	Class 1	> 10	1991
681/2506	9	BOURNEMOUTH BC	SZ18069060	SZ18009049	0.13	Gabions	Class 2	> 10	1987
681/2507	_	1 BOURNEMOUTH BC	SZ17829039	SZ17839019	0.20	Groynes	Class 2	v 10	1938
681/2507	2	BOURNEMOUTH BC	SZ17829039	SZ17839019	0.20	Armour	Class 2	> 10	1987
681/2508	_	BOURNEMOUTH BC	SZ17829039	SZ16509077	1.46	Beach Ridge			
681/2508	7	BOURNEMOUTH BC	SZ17829039	SZ16509077	1.46	Cliff / Scarp			
681/2509	-	BC	SZ16509077	SZ16129085	0.37	Groynes	Class 2	> 10	1987
681/2509	2	BOURNEMOUTH BC	SZ16519076	SZ16319081	0.21	Gabions	Class 2	> 10	1987
681/2509	က	BOURNEMOUTH BC	SZ16509077	SZ16129083	0.37	Recharge	Class 2	5 - 10	1988
681/2510	_	BOURNEMOUTH BC	SZ15959090	SZ15769093	0.19	Groynes	Class 2	5 - 10	1987
681/2510	2	BOURNEMOUTH BC	SZ15389097	SZ15569097	0.02	Groynes	Class 2	5 - 10	1976
681/2510	က	BOURNEMOUTH BC	SZ16129085	SZ15329099	0.81	Recharge	Class 2	5 - 10	1988
681/2510	4	BOURNEMOUTH BC		SZ15679095	0.10	Gabions	Class 2	5 - 10	1987
681/2511		BOURNEMOUTH BC	SZ15329099	SZ14919105	0.41	Revetment	Class 2	> 10	1958

Defence	Sub	Ownership/	<b>Grid Ref Star</b>	Grid Ref Start Grid Ref End	Defence	Structure Type	Condition	Residual	Year
Code	e Code	Responsibility	Coords	Coords	Length (km)	:		Life	
681/2511	2	2 BOURNEMOUTH BC	SZ14919105	SZ14179120	0.51	Revetment	Class 2	> 10	1975
681/2511	က	3 BOURNEMOUTH BC	SZ14179120	SZ13759124	0.73	Revetment	Class 2	> 10	1958
681/2511	4	4 BOURNEMOUTH BC	SZ13759124	SZ12989127	0.74	Revetment	Class 2	> 10	1935
681/2511	2		SZ12989127	SZ12029124	76.0	Revetment	Class 2	> 10	1932
681/2511	ပ	BOURNEMOUTH	SZ12029124	SZ11179114	0.84	Revetment	Class 2	> 10	1927
681/2511	7		SZ15329099	SZ11159114	4.20	Groynes	Class 2	5 - 10	1980
681/2511	∞	BOURNEMOUTH BC	SZ15329099	SZ11159114	4.20	Recharge	Class 2	5 - 10	1989
681/2511	6	9 BOURNEMOUTH BC	SZ15329099	SZ11159114	4.20	Splash Wall	Class 2	> 10	1930
681/2511	9	10 BOURNEMOUTH BC	SZ11179114	SZ11199096	0.18	Groynes	Class 4	< 5	1930
681/2511	7	11 BOURNEMOUTH BC	SZ12029124	SZ11159114	0.07	Wall	Class 2	> 10	1927
681/2512	-	BOURNEMOUTH BC	SZ11159114	SZ09659091	1.58	Revetment	Class 2	> 10	1911
681/2512	2	BOURNEMOUTH BC	SZ09659091	SZ08909077	0.80	Revetment	Class 2	> 10	1907
681/2512	က	200	SZ09659091	SZ09909096	0.55	Toe Piling	Class 2	> 10	1972
681/2512	4	BOURNEMOUTH BC	SZ11159114	SZ08859067	2.49	Groynes	Class 2	> 10	1980
681/2512	2	BOURNEMOUTH BC	SZ11159114	SZ08859067	2.49	Groynes	Class 2	> 10	1970
681/2512	ဖ	BOURNEMOUTH BC	SZ11159114	SZ08859067	2.49	Splash Wall	Class 2	> 10	1970
681/2512			SZ11159114	SZ08859067	2.49	Recharge	Class 2	5 - 10	1989
681/2512		ULVERT	SZ08909067	SZ08979068	0.30	Groynes	Class 3	> 10	1972
681/2512	<b>ග</b>		SZ08959067	SZ08889067	0.11	Wall	Class 2	> 10	1930
681/2513			SZ08959067	SZ08509057	0.40	Revetment	Class 2	> 10	1909
681/2513			SZ08509057	SZ07969039	0.57	Revetment	Class 2	> 10	1929
681/2513	m .	1	SZ07969039	SZ07529019	0.49	Revetment	Class 2	> 10	1930
681/2513	4		SZ07529019	SZ07289008		Revetment	Class 2	> 10	1909
681/2513	ည		SZ07289006	SZ07138993	0.20	Revetment	Class 2	> 10	1957
681/2513	ဖွ	BC	SZ07279008	SZ07138993	0.20	Recurved Wall	Class 2	> 10	1957
681/2513			SZ08859067	SZ07138993	1.91	Groynes	Class 2	5 - 10	1980
681/2513	8	ВС	SZ08859067	SZ07138993	1.91	Mall	Class 1	× 10	1957
681/2513	ത		SZ08859067	SZ07138993	1.91		Class 3	5 - 10	1989
681/2601	Ŧ	ВС	SZ21839313	SZ21819312	0.7	'n	Class 1	> 10	1991
681/2601	2(	CHRISTCHURCH BC	SZ21839313	SZ21819312	0.03	Recharge	Class 1	> 10	1993

Defence	gng	Ownership/	Grid Ref Start Grid Ref End	Grid Ref End	Defence	Structure Type Condition	Condition	Residual	Year
Code	Code	Responsibility	Coords	Coords	Length (km)			Life	Built
681/2602	-	CHRISTCHURCH BC	SZ21819312	SZ20489301	1.35 F	Revetment	Class 2	> 10	1968
681/2602	2	CHRISTCHURCH BC	! !	SZ20489301	1.35	Toe Piling	Class 3		1968
681/2602	3	CHRISTCHURCH BC		SZ20489301	1.35 (	Groynes	Class 2	> 10	1992
681/2602	4	CHRISTCHURCH BC	SZ21819312	SZ20489301	1.35 F	Recharge	Class 3	5 - 10	1992
681/2602	5	CHRISTCHURCH BC		SZ20489301		Wall	Class 2	> 10	1970
681/2603	~		SZ19919290	SZ19819286	0.10	Revetment	Class 3	> 10	1989
681/2603	2		SZ19919290	SZ19819286	0.10	Recharge	Class 3	> 10	1989
681/2604	Ψ.	CHRISTCHURCH BC	SZ19819286	SZ19479273	0.31	Recurved Wall	Class 2	> 10	1960
681/2604	2	CHRISTCHURCH BC		SZ19479273	0.31	Toe Piling	Class 3	5 - 10	1960
681/2604	က	CHRISTCHURCH BC	SZ19819286	SZ19479273	0.31	Groynes	Class 4	5 - 10	1900
681/2605	1	CHRISTCHURCH BC		SZ19169252	0.38	Revetment	Class 3	5 - 10	1960
681/2605	2	CHRISTCHURCH BC	SZ19479273	SZ19169252	0.38	Groynes	Class 2	> 10	1979
681/2605	3	CHRISTCHURCH BC	SZ19479273	SZ19169252	0.38	Toe Piling	Class 2	> 10	1979
681/2605	4	4 CHRISTCHURCH BC		SZ19169252	0.38	Revetment	Class 2	> 10	1979
681/2606	-7	CHRISTCHURCH BC	SZ19169252	SZ18909224	0.38	Wall	Class 2	> 10	1960
681/2606	7	CHRISTCHURCH BC		SZ18909224	0.38	Groynes	Class 2	> 10	1984
681/2606	က	CHRISTCHURCH BC		SZ19049243	0.14 \	Wall	Class 2	> 10	1960
681/2606	4	CHRISTCHURCH BC	SZ19049243	SZ18909224	0.24	Splash Wall	Class 2	> 10	1960
681/2607		CHRISTCHURCH BC		SZ18799207	0.21	Wall	Class 2	> 10	1960
681/2607	2	CHRISTCHURCH BC		SZ18799207		Groynes	Class 2	> 10	1988
681/2607	3	CHRISTCHURCH BC		SZ18799207	0.21	Recharge	Class 2	> 10	1988
681/2608	_			SZ18549182	0.38	Wall	Class 2	> 10	1978
681/2608	2	CHRISTCHURCH BC		SZ18549182	0.38	Toe Piling	Class 2		1978
681/2608	3	CHRISTCHURCH BC	SZ18799207	SZ18549182	0.38	Groynes	Class 2	> 10	1978
681/2608	4	CHRISTCHURCH BC		SZ18549182	0.38	Splash Wall	Class 2	> 10	1978
681/2608	5	CHRISTCHURCH BC	SZ18799207	SZ18549182	0.38	Apron	Class 2		1978
681/2609	~	CHRISTCHURCH BC	SZ18549182	SZ18409157	0.40 F	Piling	Class 1	> 10	1996
681/2609	7	CHRISTCHURCH BC		SZ18389164	0.03 F		Class 1	× 10	1996
681/2609	က	CHRISTCHURCH BC		SZ18379163	0.02 F		Class 1	> 10	1996
681/2609	4	CHRISTCHURCH BC	SZ18379163	SZ18319158	0.08 F	Piling	Class 1	> 10	1996

Defence	Sub	Defence Sub Ownership/	Grid Ref Start	Grid Ref End	Defence S	Grid Ref Start Grid Ref End Defence   Structure Type   Condition   Residual	Condition	Residual	Vear
Code	Code	Responsibility	Coords	Coords	Length (km)			Life	Built
681/2609	2	5 CHRISTCHURCH BC	SZ18319158 SZ18279163	SZ18279163	0.07 F		Class 1	> 10	1996
681/2609	9	6 CHRISTCHURCH BC	SZ18279163	SZ18289164	0.02 F		Class 1	× 10	1006
681/2609	7	CHRISTCHURCH BC	SZ18289158	SZ18289157	0.01		Class 1	10 ×	1906
681/2610	_	CHRISTCHURCH BC		SZ18389150	0.27 E	0.27 Bank		>	3
681/2611	*-	CHRISTCHURCH BC		SZ18379135	0.19 F	-	Class 2	> 10	1980
681/2611	2	CHRISTCHURCH BC		SZ18379150	0.19		Class 2	10	1080
681/2612		CHRISTCHURCH BC	SZ18289147	SZ18389150	0.20 E	0.20 Beach Ridge		2	3

# Appendix B

